

次世代観測装置用の新しい 回折格子の開発状況

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Volume Phase Holographic Grating



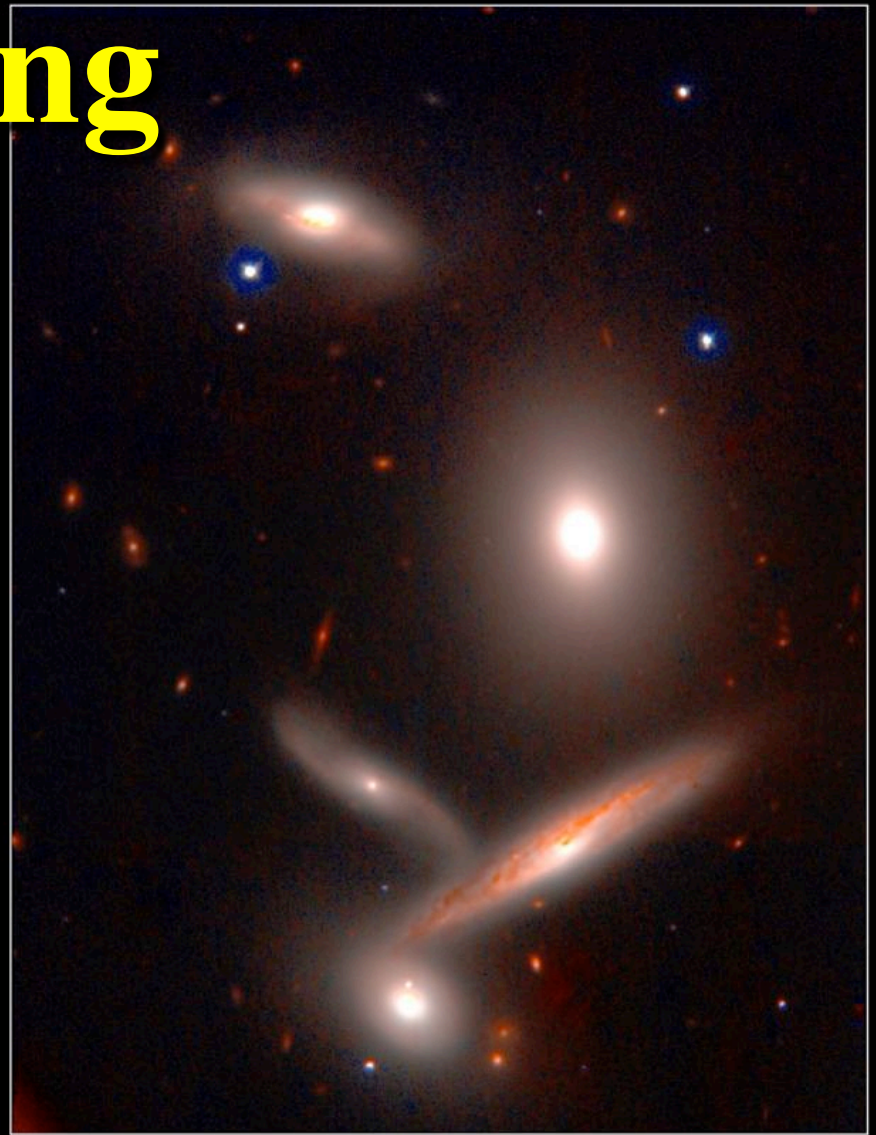
M 82 (NGC 3034)

Subaru Telescope, National Astronomical Observatory of Japan

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FOCAS (B, V, H α)

March 24, 2000



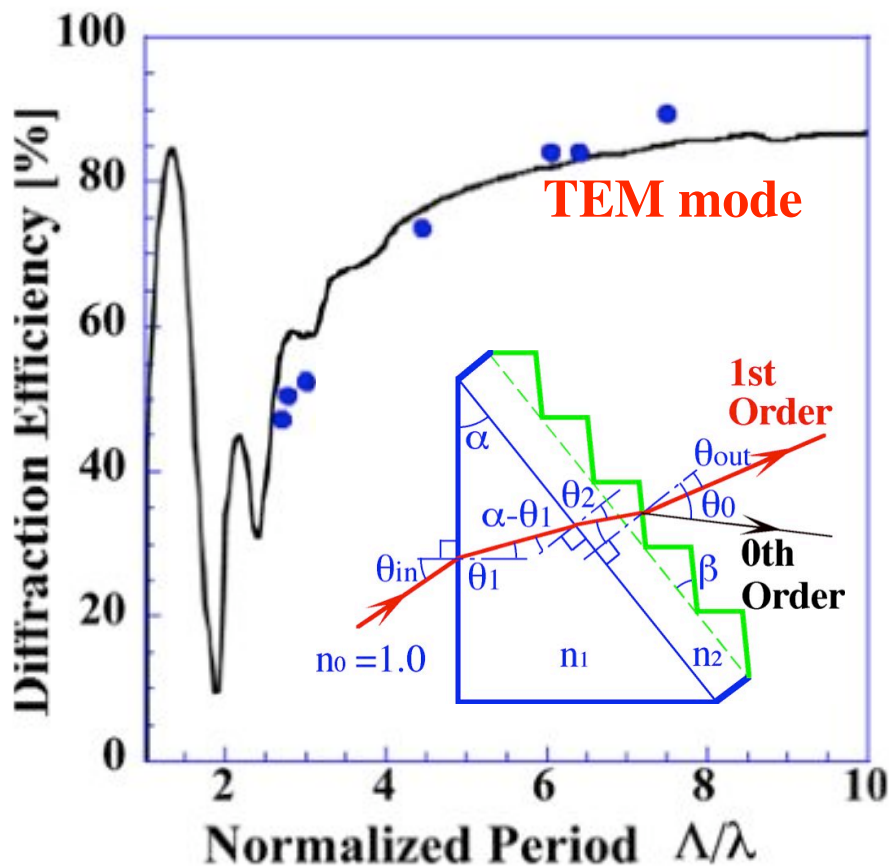
Hickson Compact Group 40

Subaru Telescope, National Astronomical Observatory of Japan

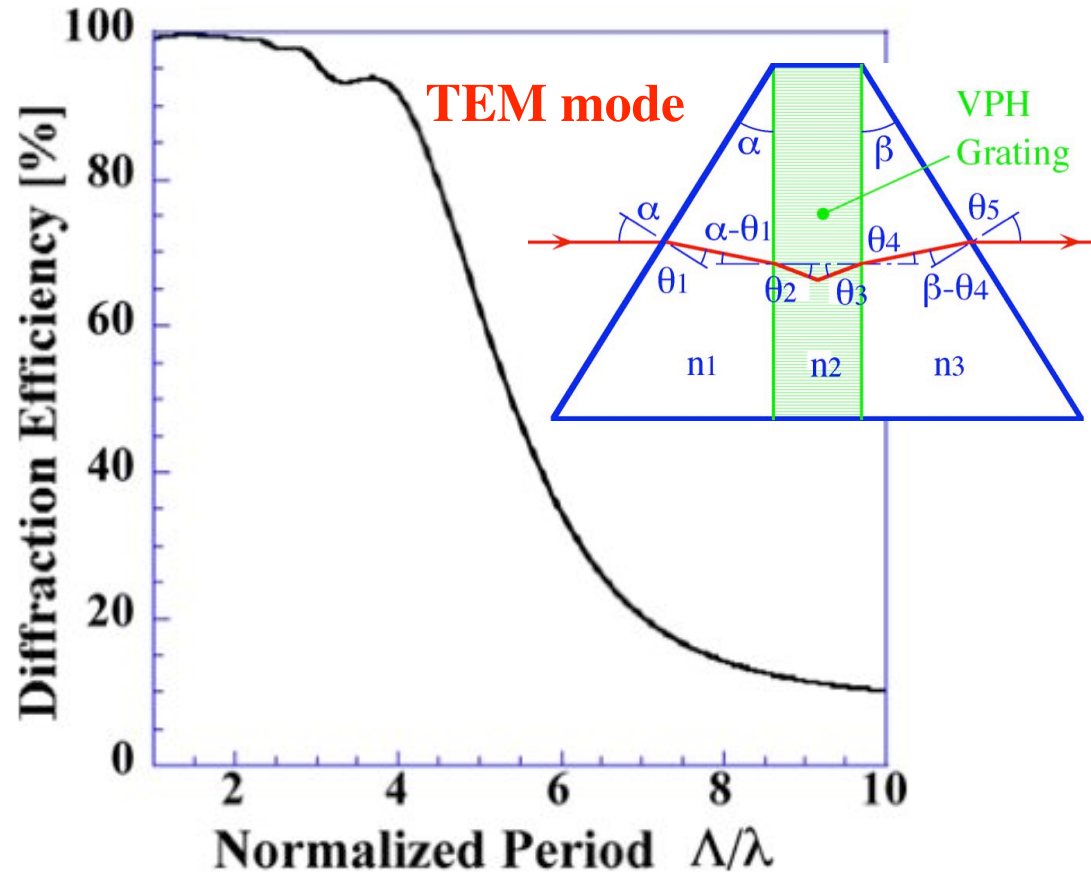
CISCO (J & K')

January 28, 1999

Efficiencies of Transmission Gratings

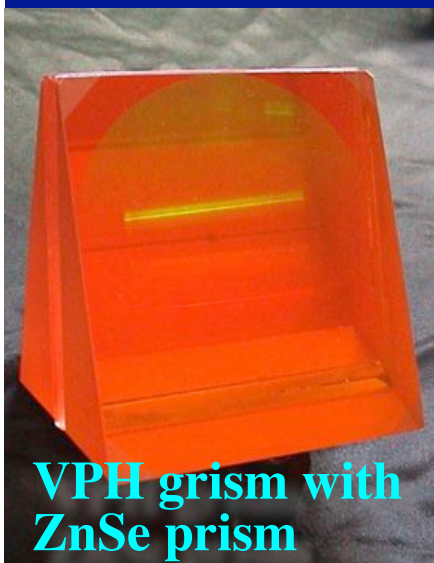


Surface relief grating:
 Efficiency decreases
 steeply below $4 \Lambda/\lambda$.

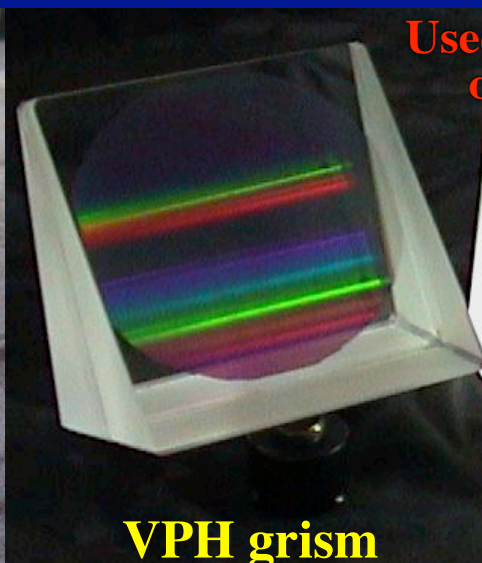


VPH (Volume Phase Holographic) grating ($\Delta n \sim 0.02$): Efficiency increases up to **100%** below $4 \Lambda/\lambda$.

(Oka et. al., SPIE, **5005**, 2003)

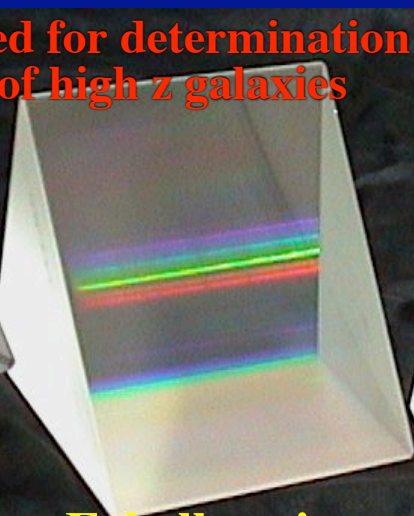


VPH grism with ZnSe prism

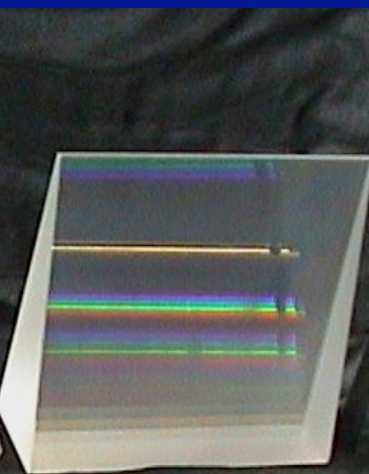


VPH grism

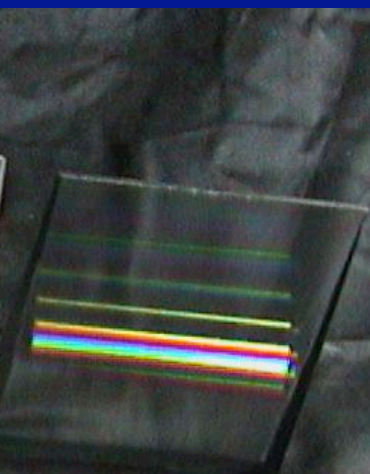
Used for determination of high z galaxies



Echelle grism



Surface relief grism



FOCAS Grisms

Size: $110 \times 106 \times 106$ (max).

4 SR grisms: $300 < R < 1,400$.

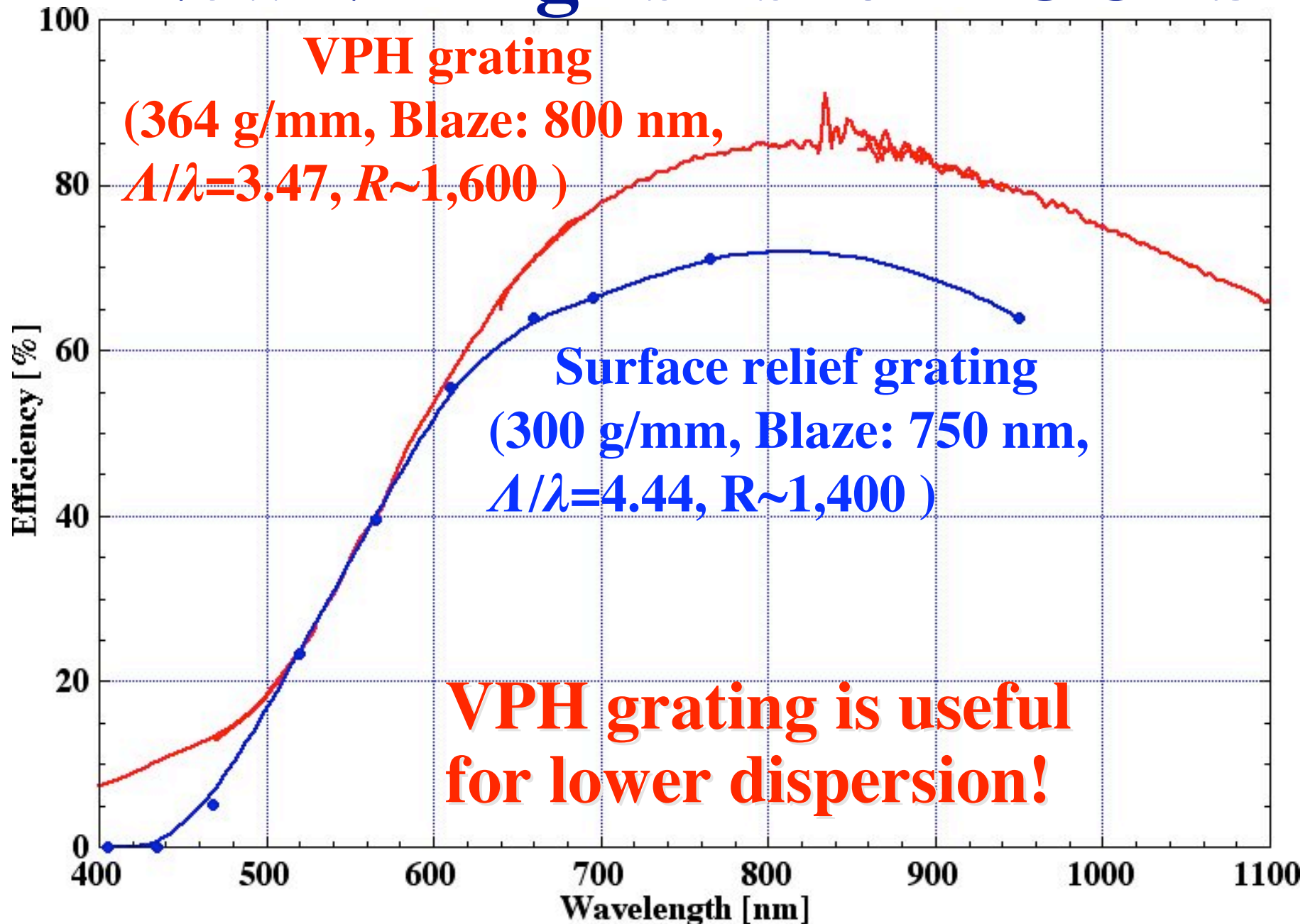
1 Echelle grism: $R \sim 2,500$.

8 VPH grisms (3 grisms with ZnSe prisms): $1,600 < R < 7,000$,
Collaboration of JWU (Japan Women's Univ.) and NAOJ.

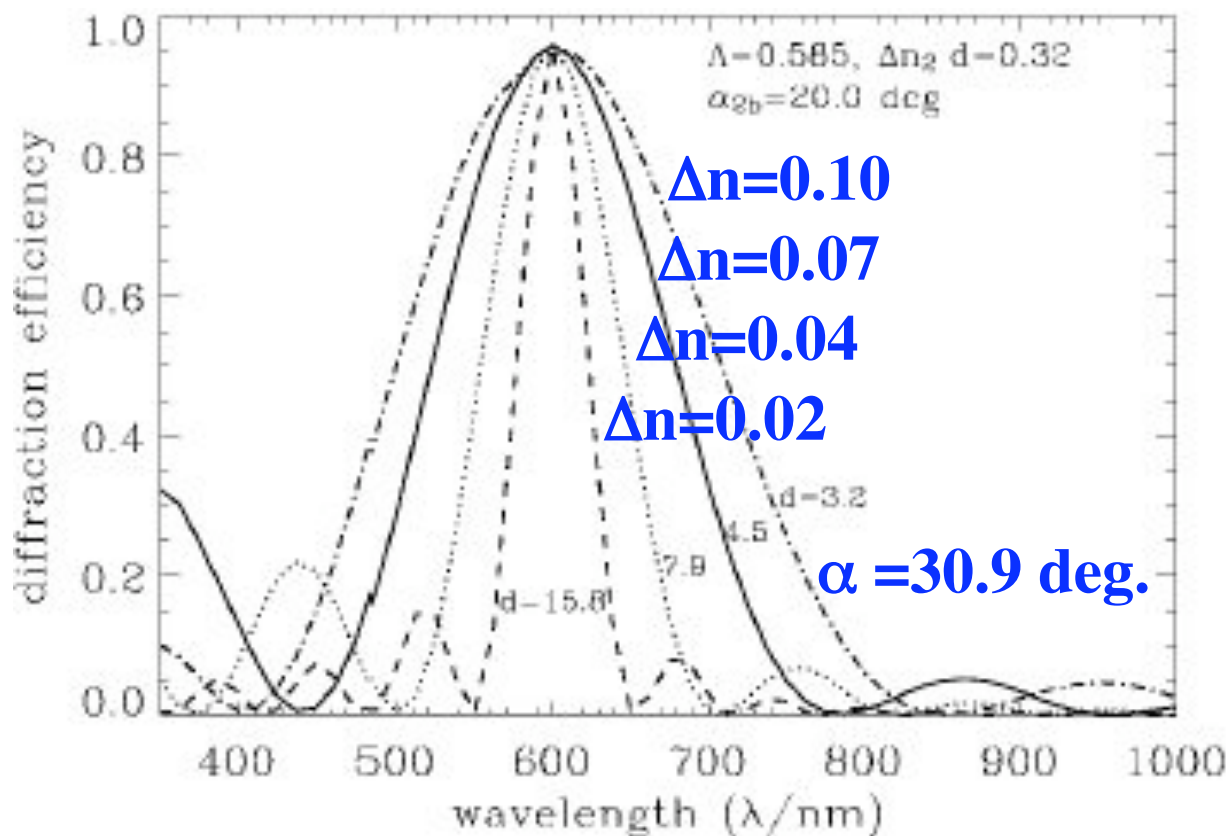
(Ebizuka et. al. PASJ, 63, 2011a)



New VPH gratings for FOCAS

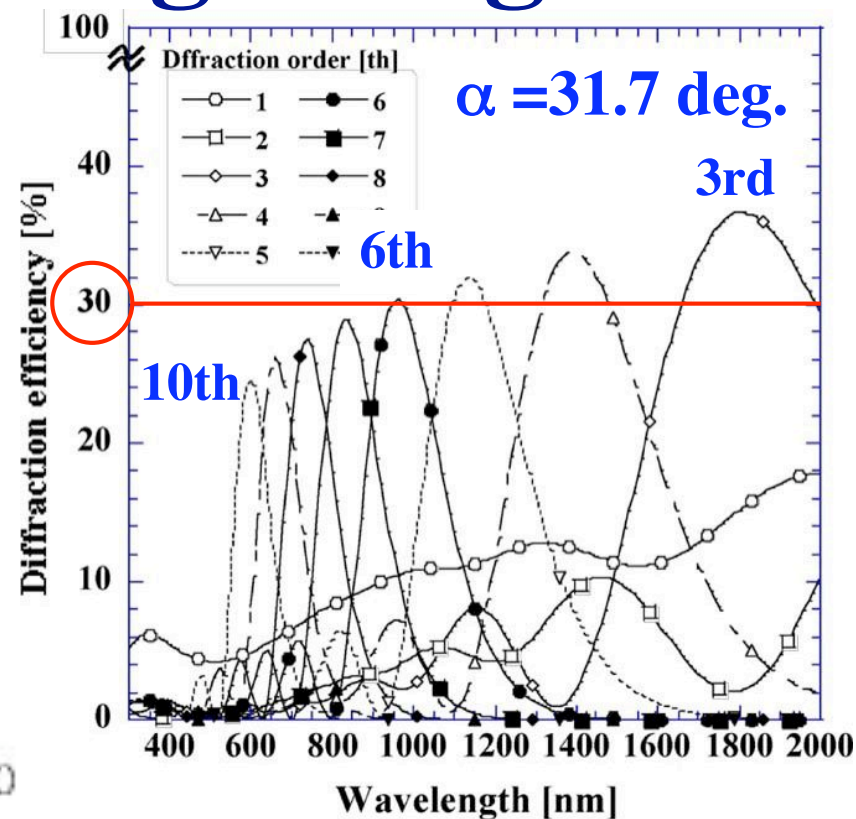


Limitation of VPH grating



Band width of VPH grating becomes narrow in diffraction angle: α increase because semi-amplitude of index modulation of dichromated gelatin (DCG) is $\Delta n < 0.15$.

(Baldry et al., PASP, 116, 2004)



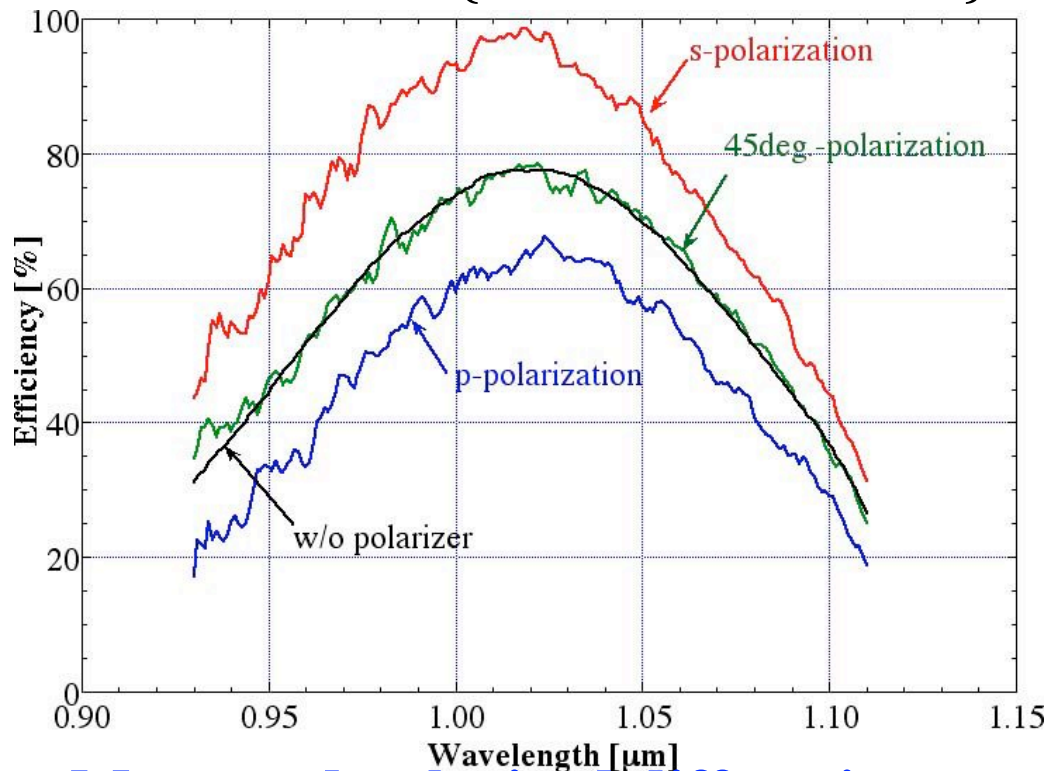
Diffraction efficiency of VPH grating decrease toward higher orders.

(Oka et. al., SPIE, 5290, 2004)

Polarized Diffraction Efficiency of VPH Grating

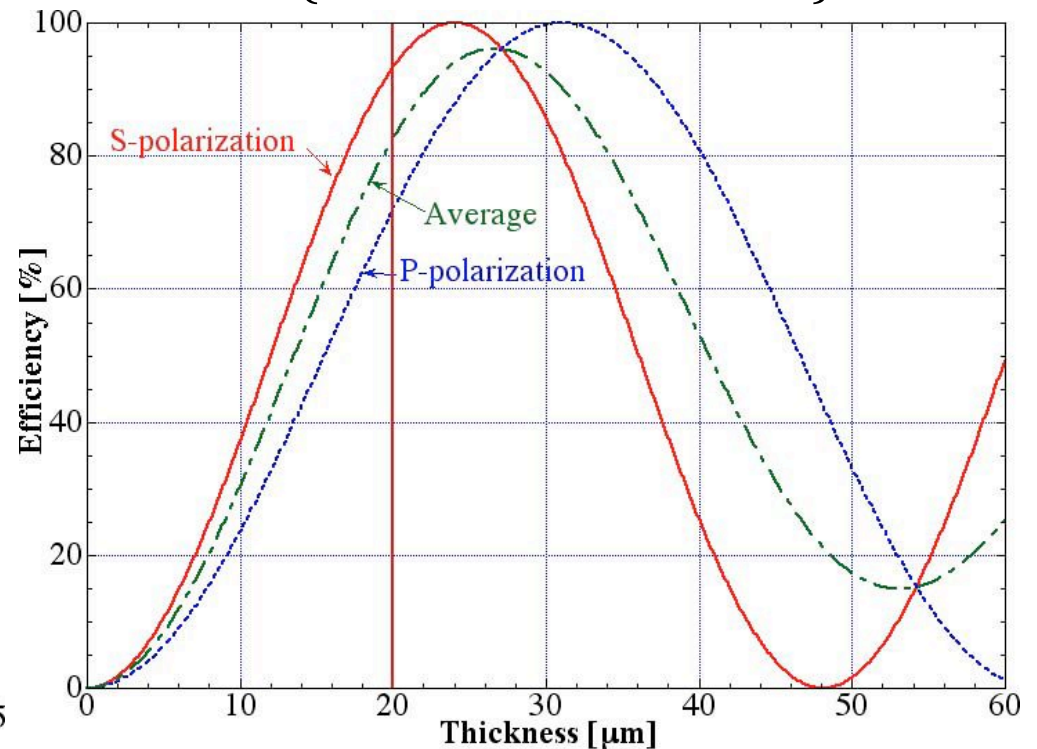
$$\eta_S = \sin^2 \left\{ \frac{\pi(n_{\max} - n_{\min})t}{\Lambda(n_{\max} + n_{\min})\sin 2\theta} \right\}$$

$$\eta_P = \sin^2 \left\{ \frac{\pi(n_{\max} - n_{\min})t \cos 2\theta}{\Lambda(n_{\max} + n_{\min})\sin 2\theta} \right\}$$



Measured polarized diffraction efficiencies of VPH grating.

$n_{\text{ave}} = (n_{\max} - n_{\min})/2 = 1.53$,
 $\Lambda = 0.984 \mu\text{m}$, $t = 20 \mu\text{m}$,
 $\theta = 19.8^\circ @ 1.02 \mu\text{m}$.



Calculated polarization diffraction efficiencies vs. t of a VPH grating.

$\Delta n = (n_{\max} - n_{\min})/2 = 0.017$

(Ebizuka et. al. PASJ, **63**, 2011b)

A wide-field astronomical image of the Horse-head Nebula (IC 434) in the constellation Orion. The nebula is a dark, silhouetted structure against a reddish-pink background of interstellar dust. Several bright stars are visible, including the prominent Betelgeuse star on the right side of the nebula's head.

Volume Binary Grating



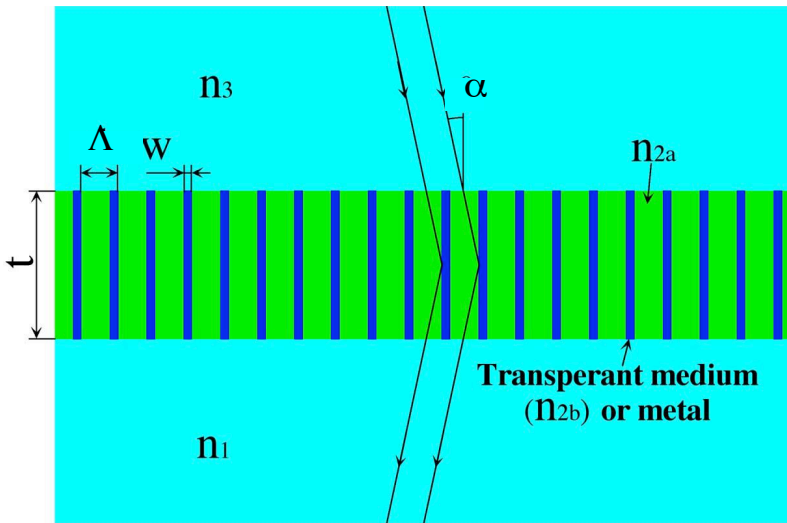
IC 434 (Horse-head Nebula)

Ultra-high-sensitivity HDTV I.I. color camera (NHK)
Exp. 22 sec. (11 frames coadded) January 16, 1999

Subaru Telescope, National Astronomical Observatory of Japan

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Volume Binary Grating



- $\Delta n = (n_{\max} - n_{\min})/2 \sim 0.5$.
- Polarized diffraction efficiencies of **S** and **P** polarization coincide with each other by tuning of f and t . While aspect ratio becomes $t : w = 1:20 \sim 100$.

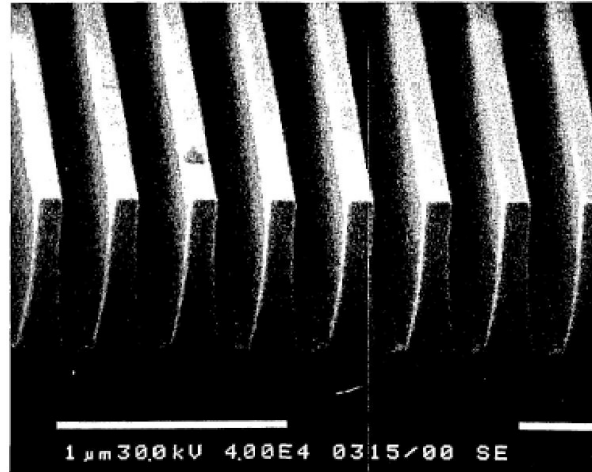


Fig. 1. Scanning electron micrograph of grating lines etched into quartz substrate ($n_s = 1.46$).

(Gerritsen, Jepsen: Appl. Opt., 37,1998)

Filling factor: $f = w/\Lambda$

$$n_H = 1.46, n_L = 1.0, \alpha = 45 \text{ deg.}$$

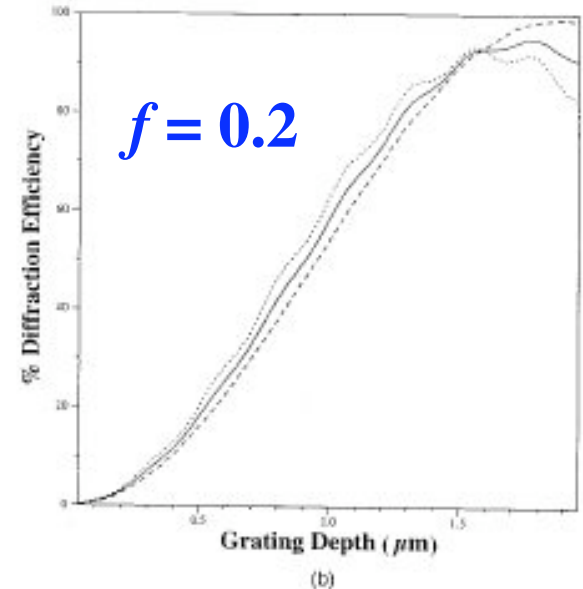
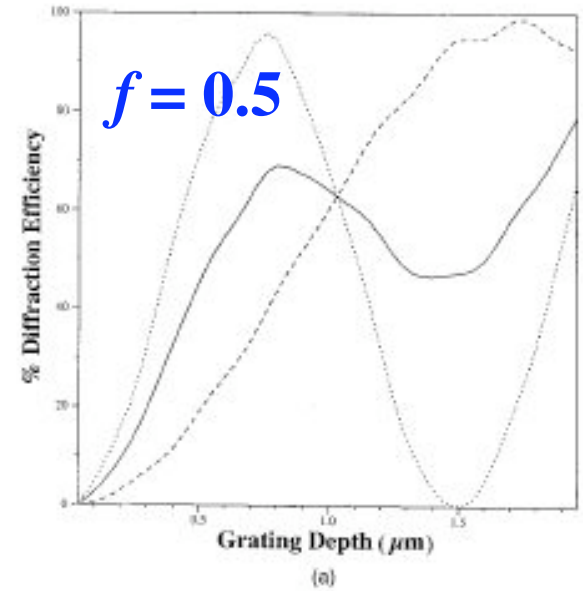
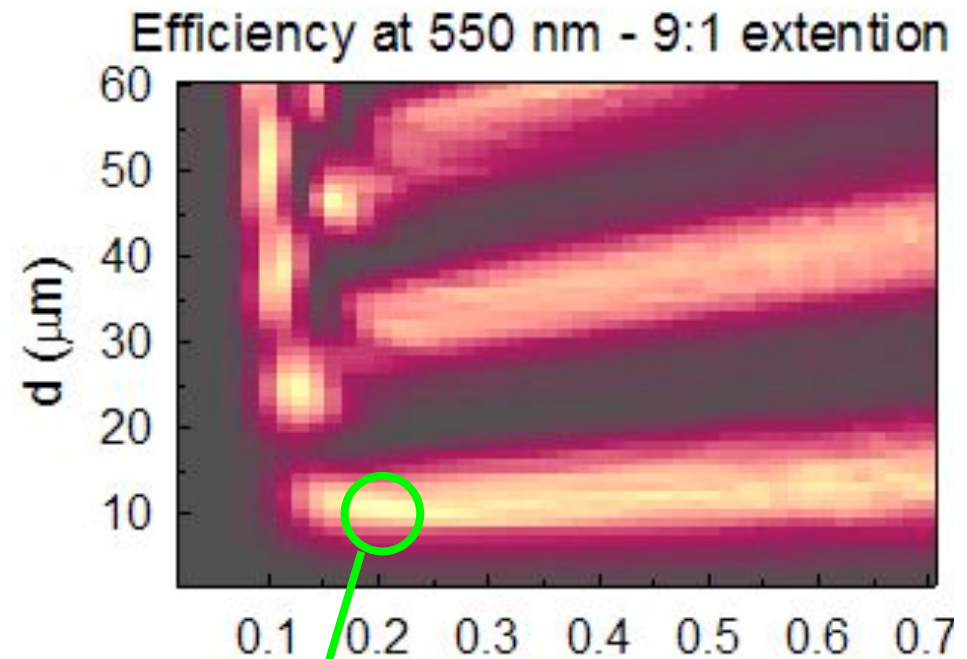
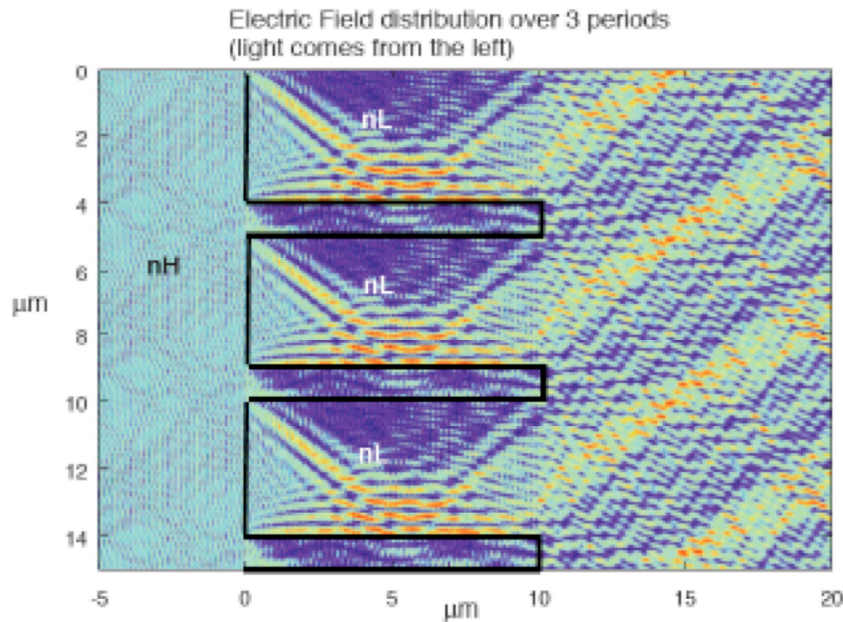


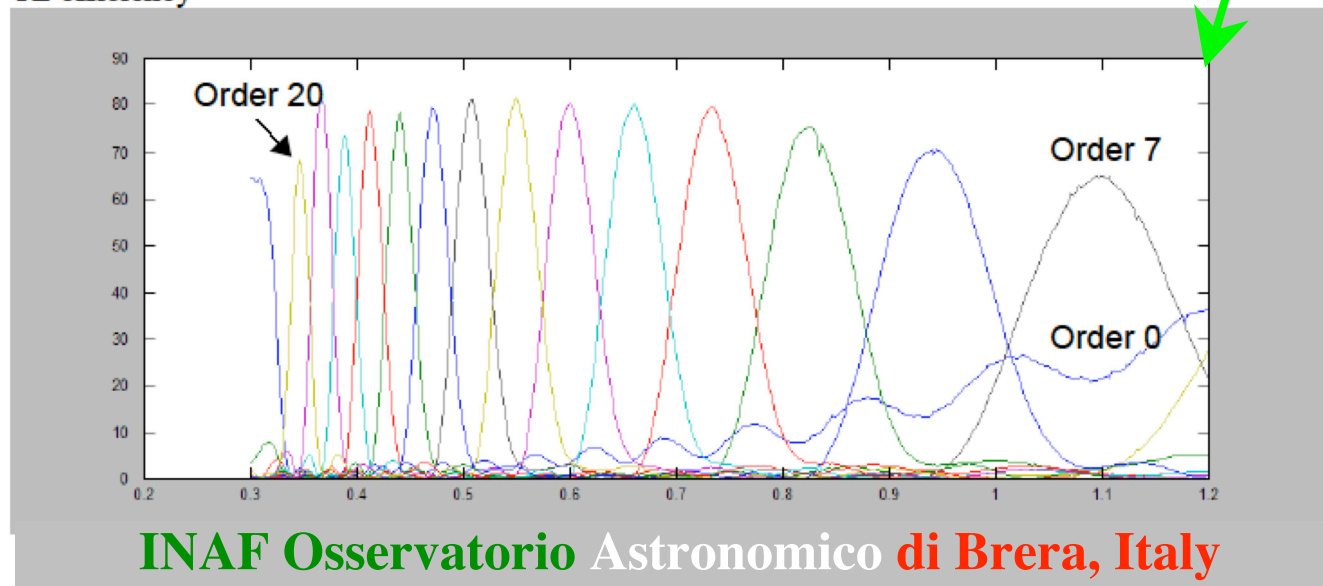
Fig. 5. (a) First-order diffraction efficiencies for a grating with $\lambda = 0.55 \mu\text{m}$, $\Lambda = 0.3889 \mu\text{m}$, $\theta_D = 45^\circ$, $n = 1.50$, and $f = 0.50$. (b) First-order diffraction efficiencies for a grating with $\lambda = 0.55 \mu\text{m}$, $\Lambda = 0.3889 \mu\text{m}$, $\theta_D = 45^\circ$, $n = 1.50$, and $f = 0.80$.

(Gupt & Peng, Appl. Opt., 32, 1993)

Volume Binary Grating for Higher Diffraction Orders



$\lambda = 0.55 \mu\text{m}$, $\alpha = 20.44^\circ (= 41.3^\circ \text{ in air})$, $n_H = 1.89$, $n_L = 1.46$, $d = 10 \mu\text{m}$
 Configuration 1: ratio 9:1, $d = 11 \mu\text{m}$, $\Delta n = 0.19$
 TE efficiency

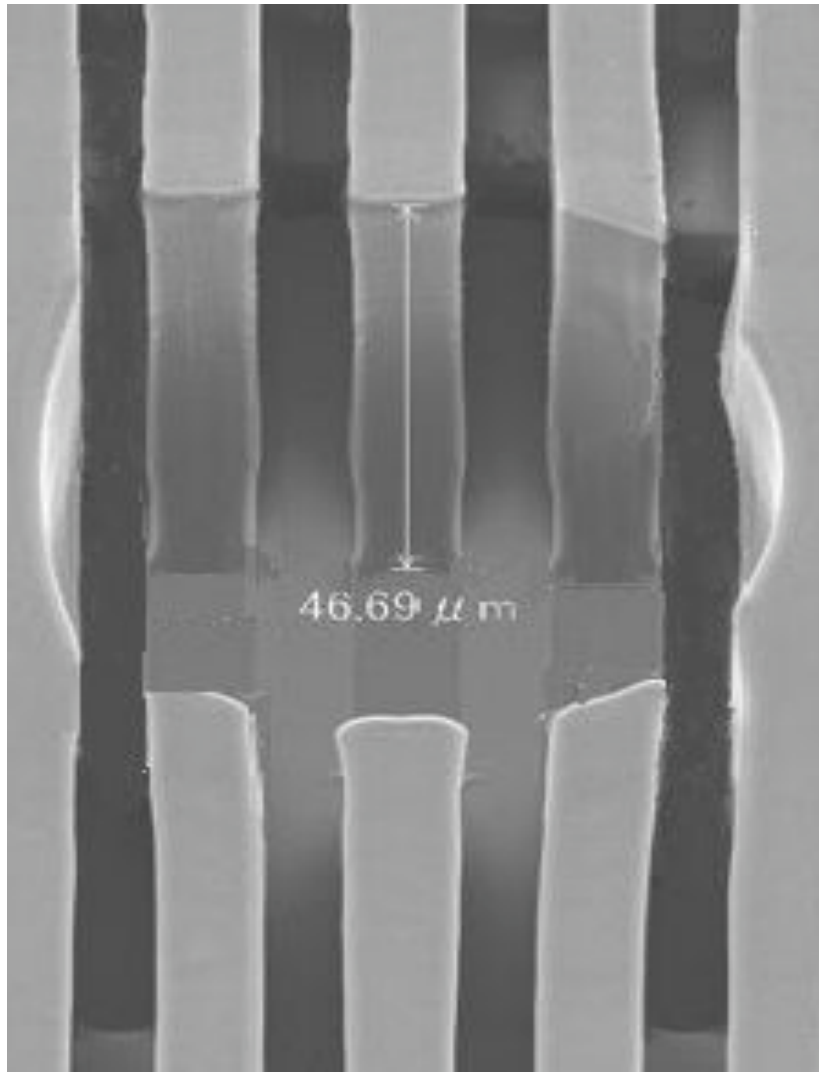


Δn
 $n_H = 1.89$, $n_L = 1.46$,
 $\alpha = 41.3^\circ$, $f = 0.1$

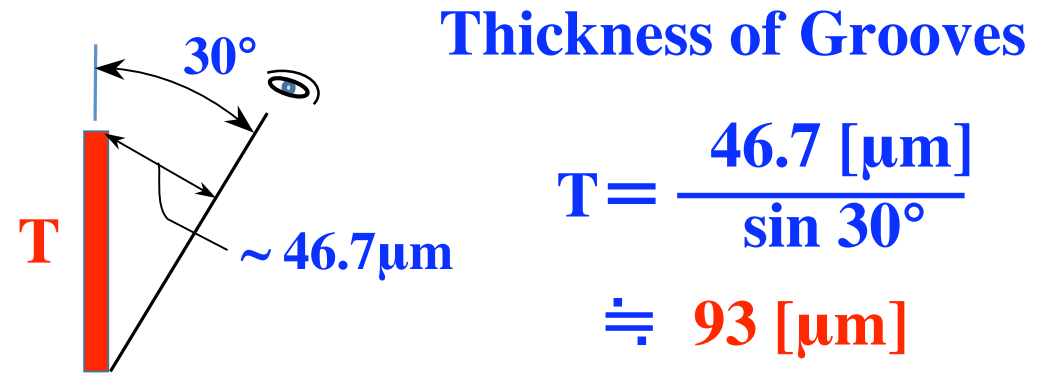
**$t:w$ (Aspect ratio)
 = 1:22**

(Bianco & Ebizuka, SPIE,
 8450, 2012)

Photo Resist Grooves with High Aspect Ratio



SEM image of grooves (L&S: 10 μm), tilting with 30°. Photo resist: KMPR1000.

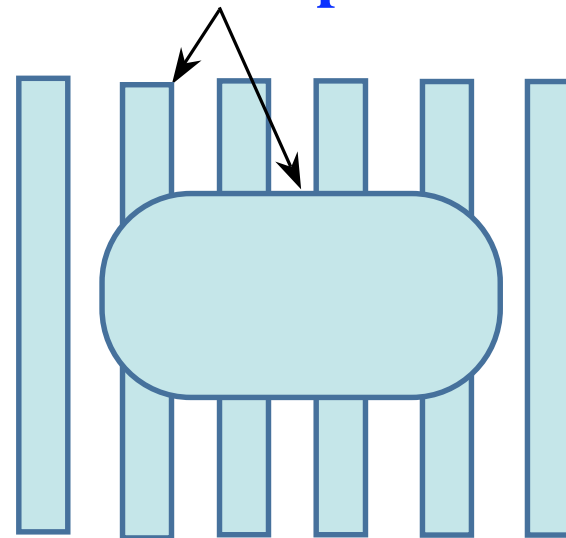


Thickness of Grooves

$$T = \frac{46.7 [\mu\text{m}]}{\sin 30^\circ}$$

$$\doteq 93 [\mu\text{m}]$$

Cr mask pattern



L&S: 10 μm \rightarrow 1 μm : 9 μm

豊田工業大学ナノテクプラットフォーム

Birefringence Volume Grating



$H\alpha$



$H\alpha, V, B$



Ring Nebula (M 57 / NGC 6720)

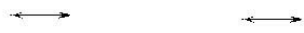
Subaru Telescope, National Astronomical Observatory of Japan

Suprime-Cam ($H\alpha, V, B$)

September 16, 1999

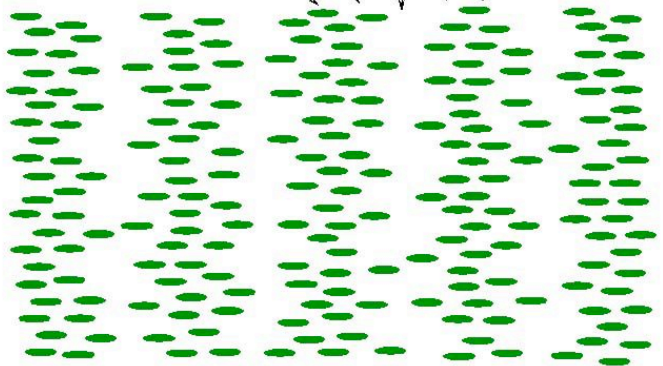
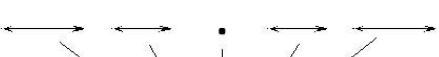
Birefringence VPH Grating

Amplitude of two beams

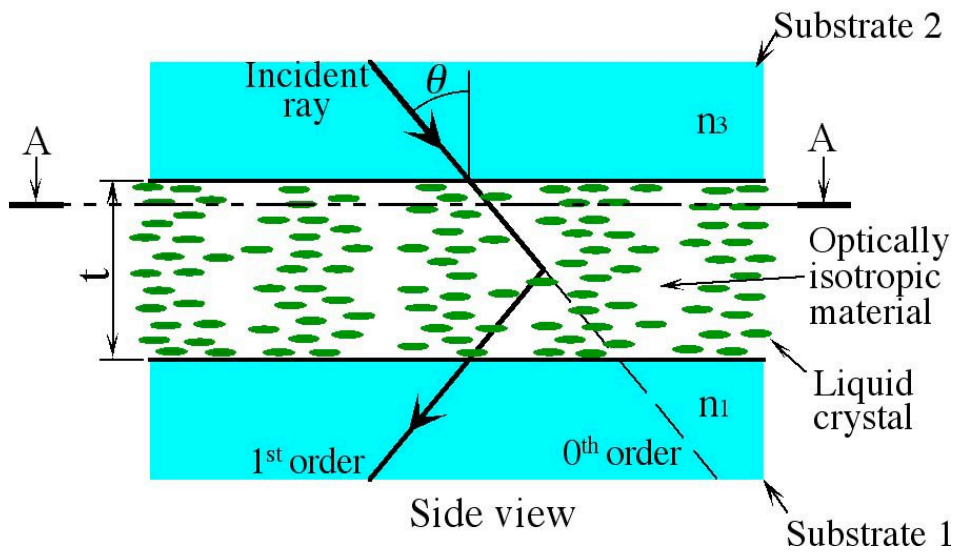


Retardation $\delta = 0 \quad \pi/2 \quad \pi \quad 3\pi/2 \quad 2\pi$

Amplitude of interferogram



Λ Cross section: A-A

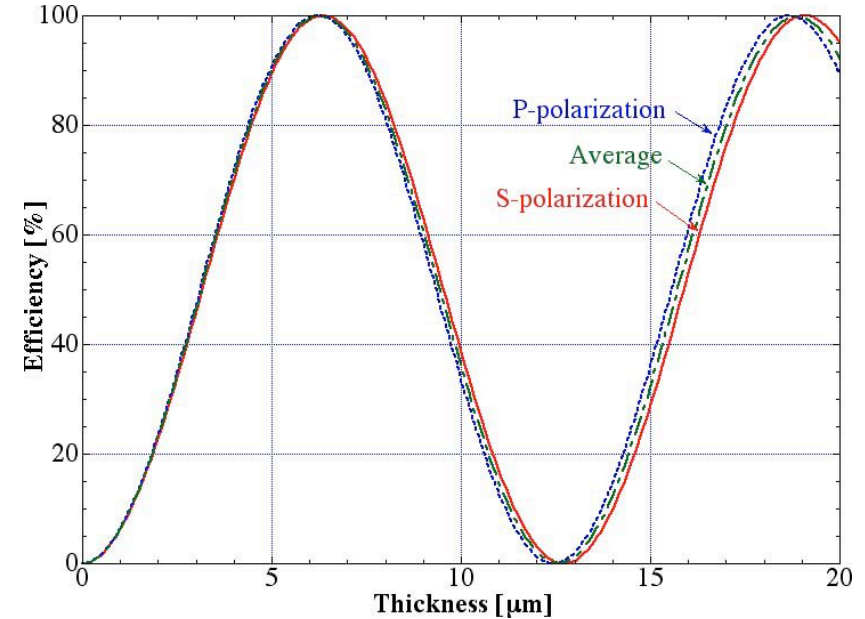


$$\frac{n_{Smax} - n_{Smin}}{(n_{Smax} + n_{Smin}) \sin 2\theta_S} = \frac{(n_{Pmax} - n_{Pmin}) \cos 2\theta_P}{(n_{Pmax} + n_{Pmin}) \sin 2\theta_P}$$

$$\frac{n_{Smax} - n_{Smin}}{(n_{Smax} + n_{Smin}) \cdot 2 \sin \theta_S \cos \theta_S} = \frac{(n_{Pmax} - n_{Pmin}) \cos 2\theta_P}{(n_{Pmax} + n_{Pmin}) \cdot 2 \sin \theta_P \cos \theta_P}$$

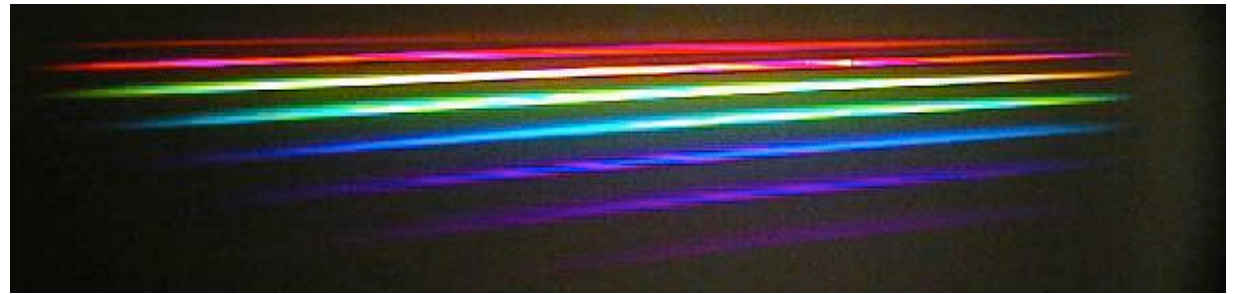
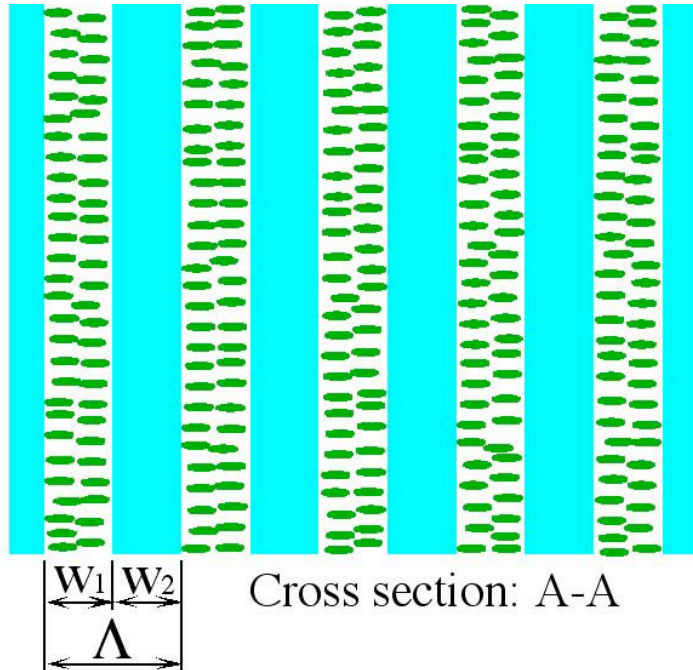
Snell's law

$$\frac{n_{Smax} - n_{Smin}}{\cos \theta_S} \cong \frac{(n_{Pmax} - n_{Pmin}) \cos 2\theta_P}{\cos \theta_P}$$



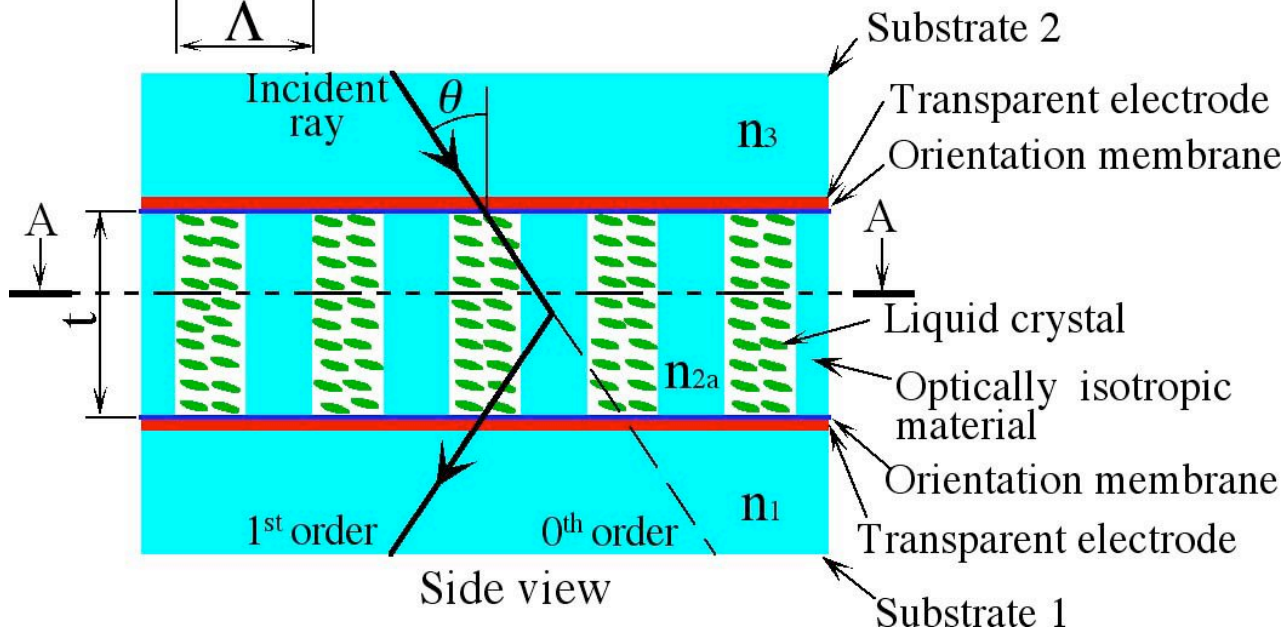
Calculated polarization diffraction efficiencies versus grating thickness t of birefringence VPH grating.

Birefringence Binary Bragg (3B) Grating



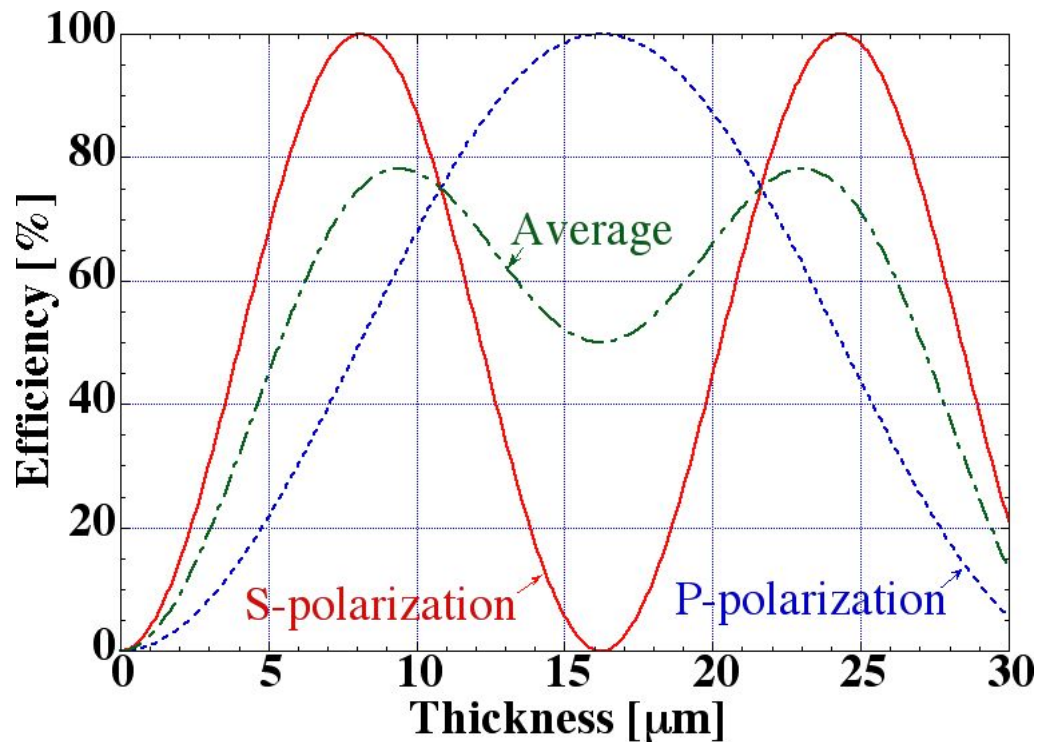
Echellegram

**High diffraction efficiency
in higher diffraction order.**

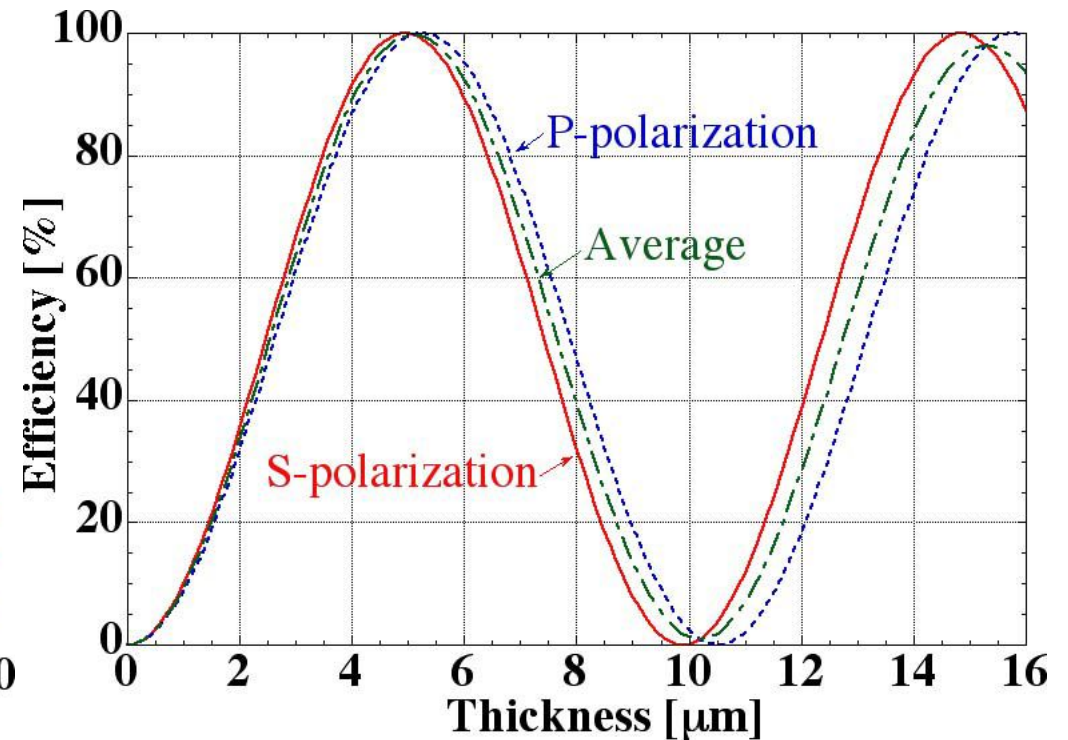


**Active optical element:
Window → Grating,
Grating → Polarizer,
Day lighting, Head-up
display, 3D display,
Optical communications
& computing, ...**

Polarized Diffraction Efficiency of VPH Grating and 3B Grating



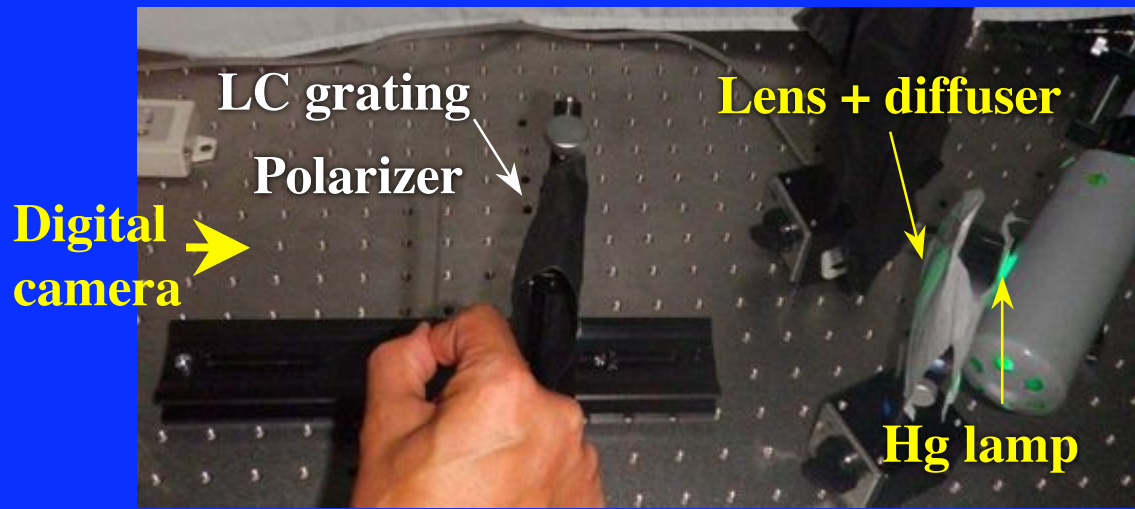
Dicson's VPH grating (Polarizer)
calculated by **Kogelnik** method.
 $n_L = 1.46$, $n_H = 1.54$, $\theta_B = 48.5^\circ$.



3B grating calculated by **RCWA**.
 $n_L = 1.46$, $n_s = 1.544$, $n_p = 1.60$, $\theta_B = 45^\circ$.

$w:t$ (Aspect ratio) = 1:20~100 \rightarrow 1:4~20

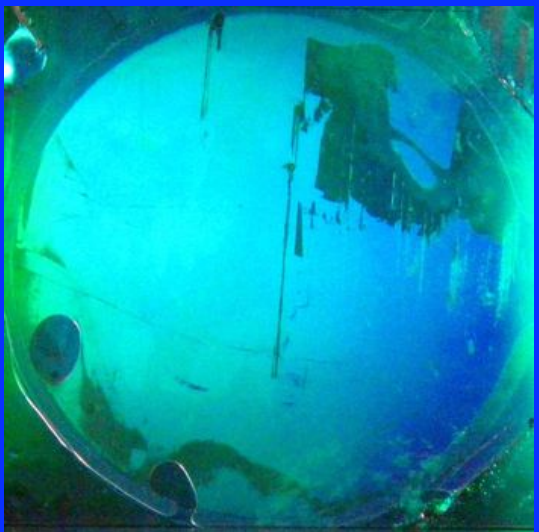
Liquid Crystal Grating (3B Grating)



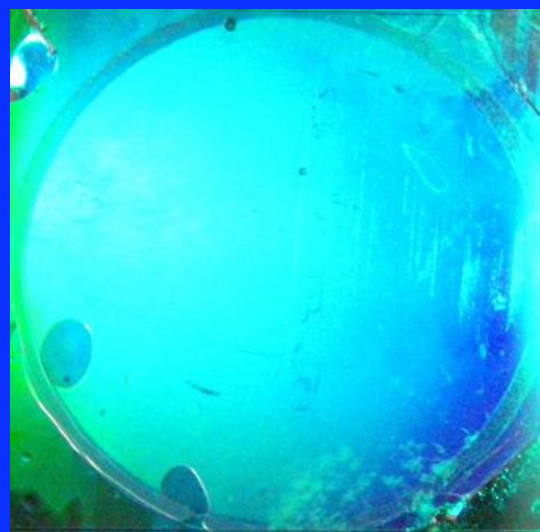
Specifications

Type: replicated grating
Groove period (Λ) : $2 \mu\text{m}$
(Line & space : $1 \mu\text{m}$)
Groove thickness (t): $1 \mu\text{m}$

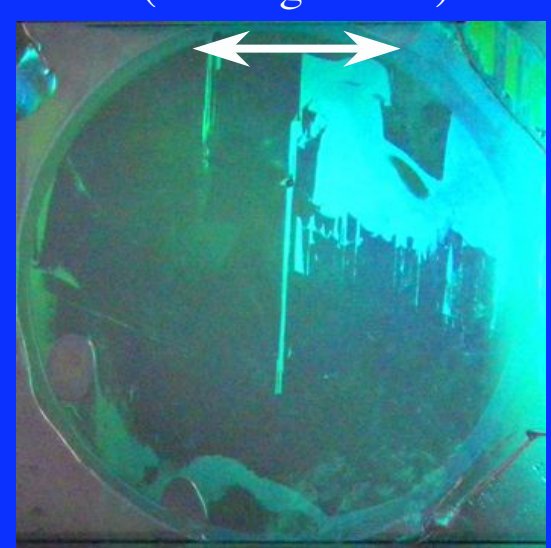
Orientation layer
(Grating vector)



Polarizer angle: $60 \sim 70^\circ$



Polarizer angle: 90°

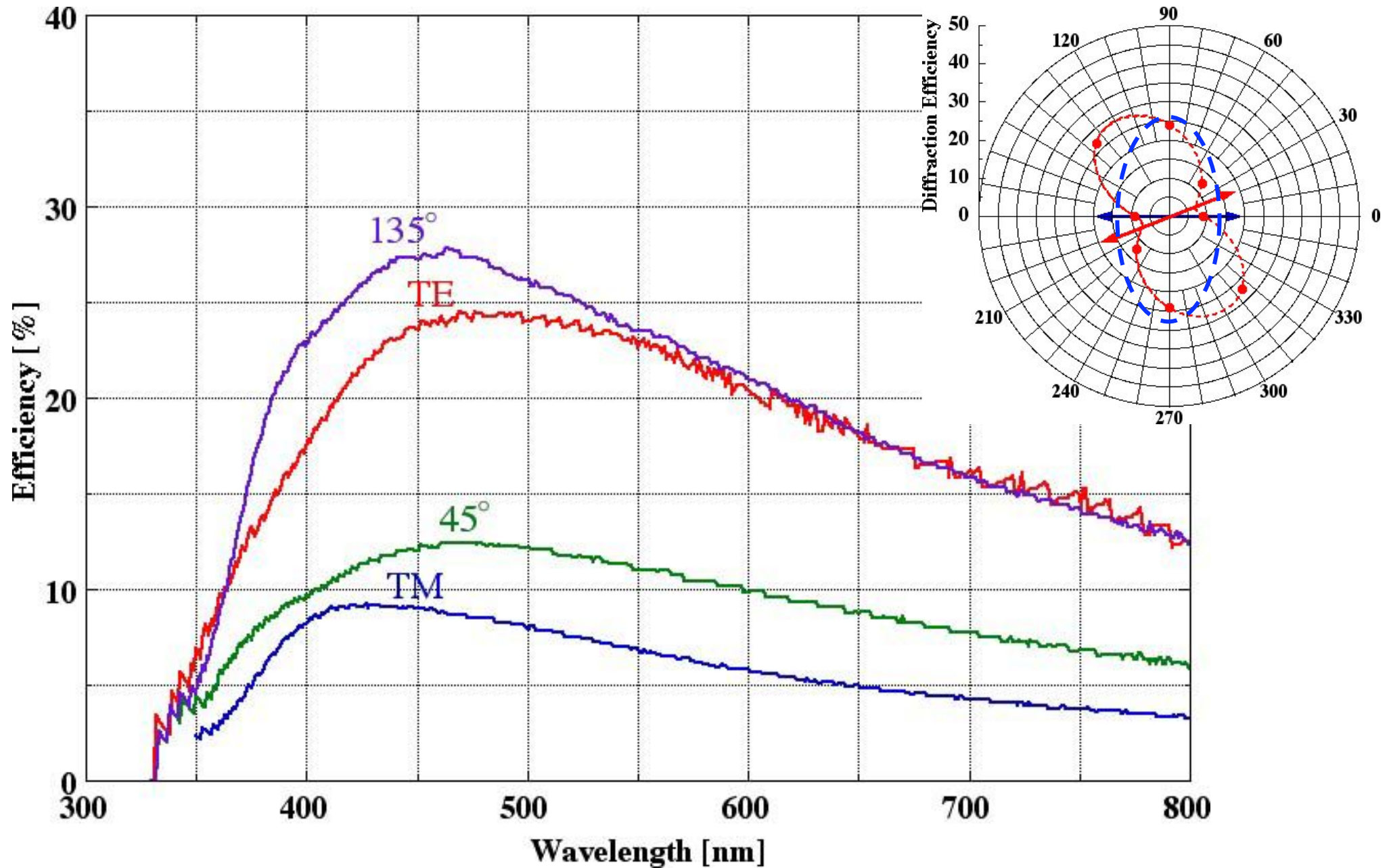


Polarizer angle: $-60 \sim -70^\circ$

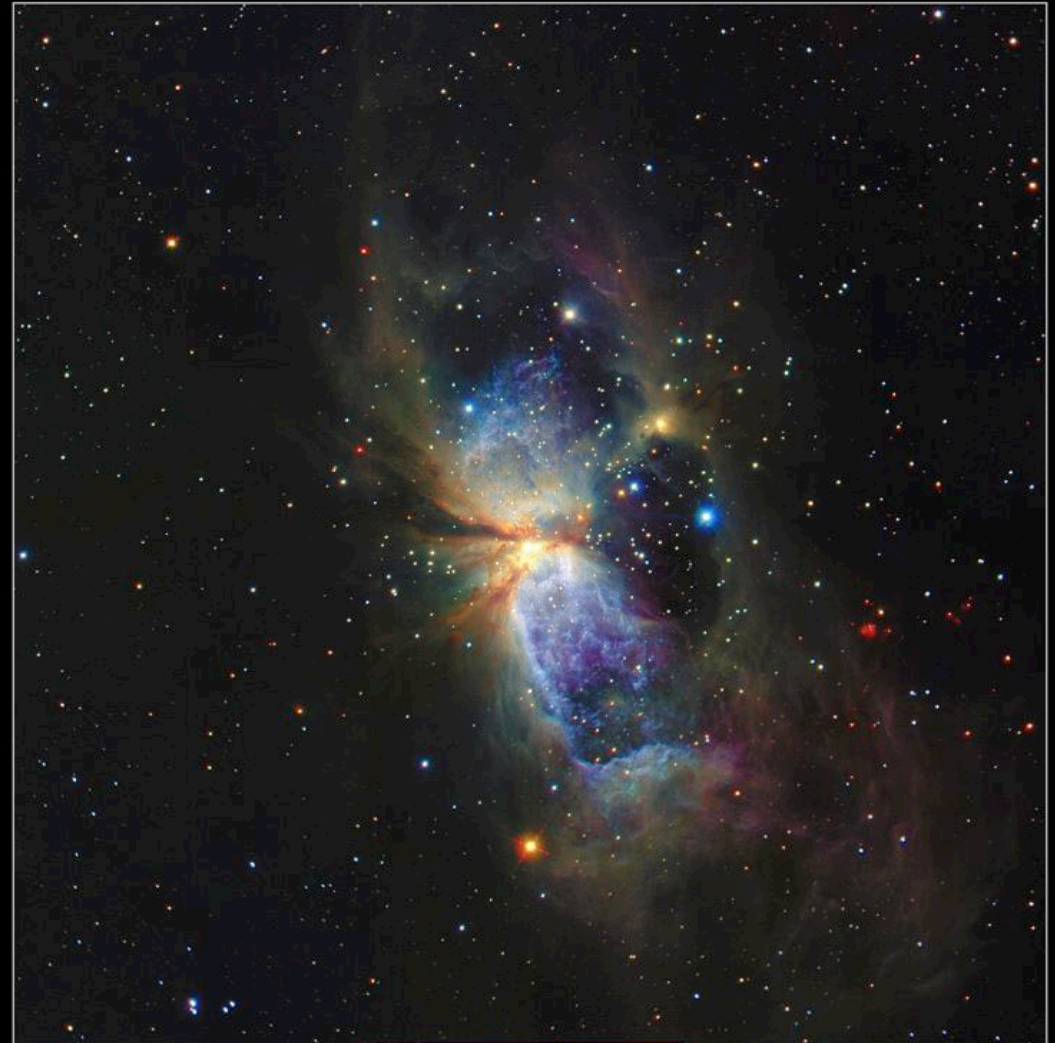
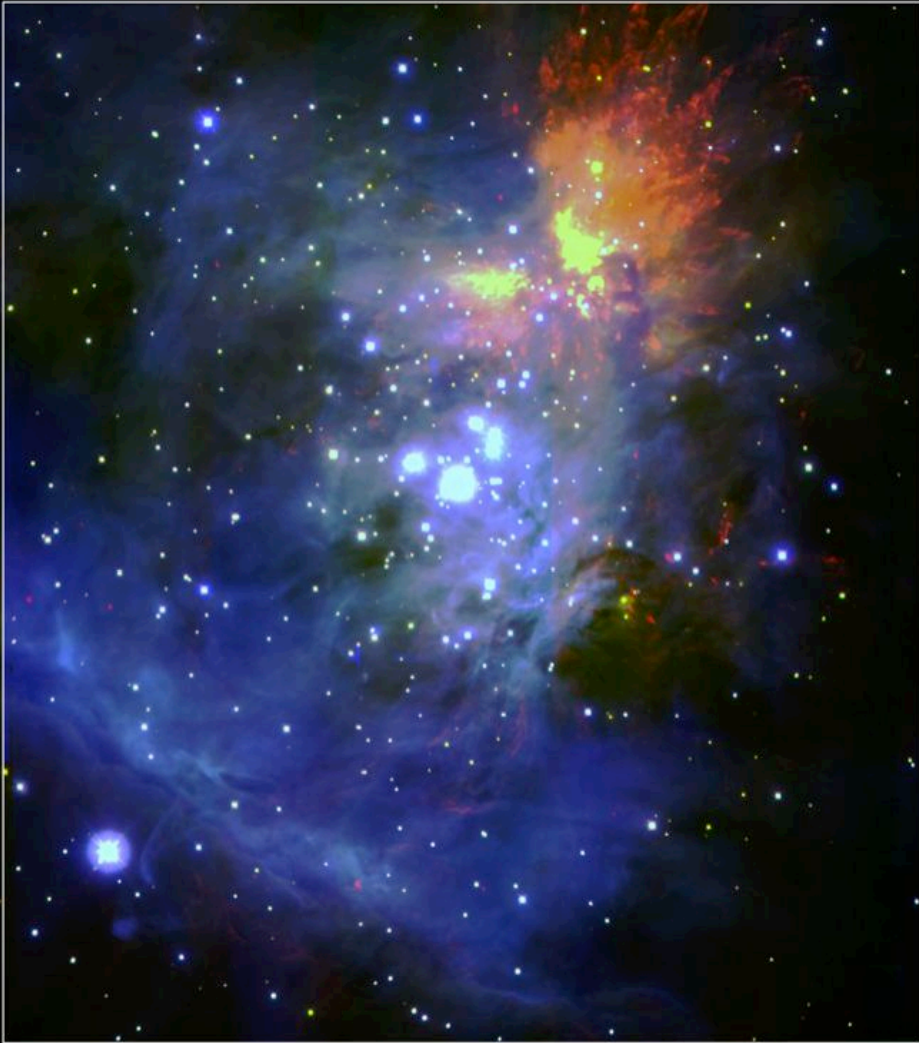
Images of the first order diffraction

シチズンホールディングス (株) 開発部

Efficiencies of Liquid Crystal (3B) Grating



Immersion Grating



Orion Nebula

Subaru Telescope, National Astronomical Observatory of Japan

CISCO (J, K' & H₂ ($v=1-0$ S(1)))

January 28, 1999



Star-forming Region S106 IRS4

Subaru Telescope, National Astronomical Observatory of Japan

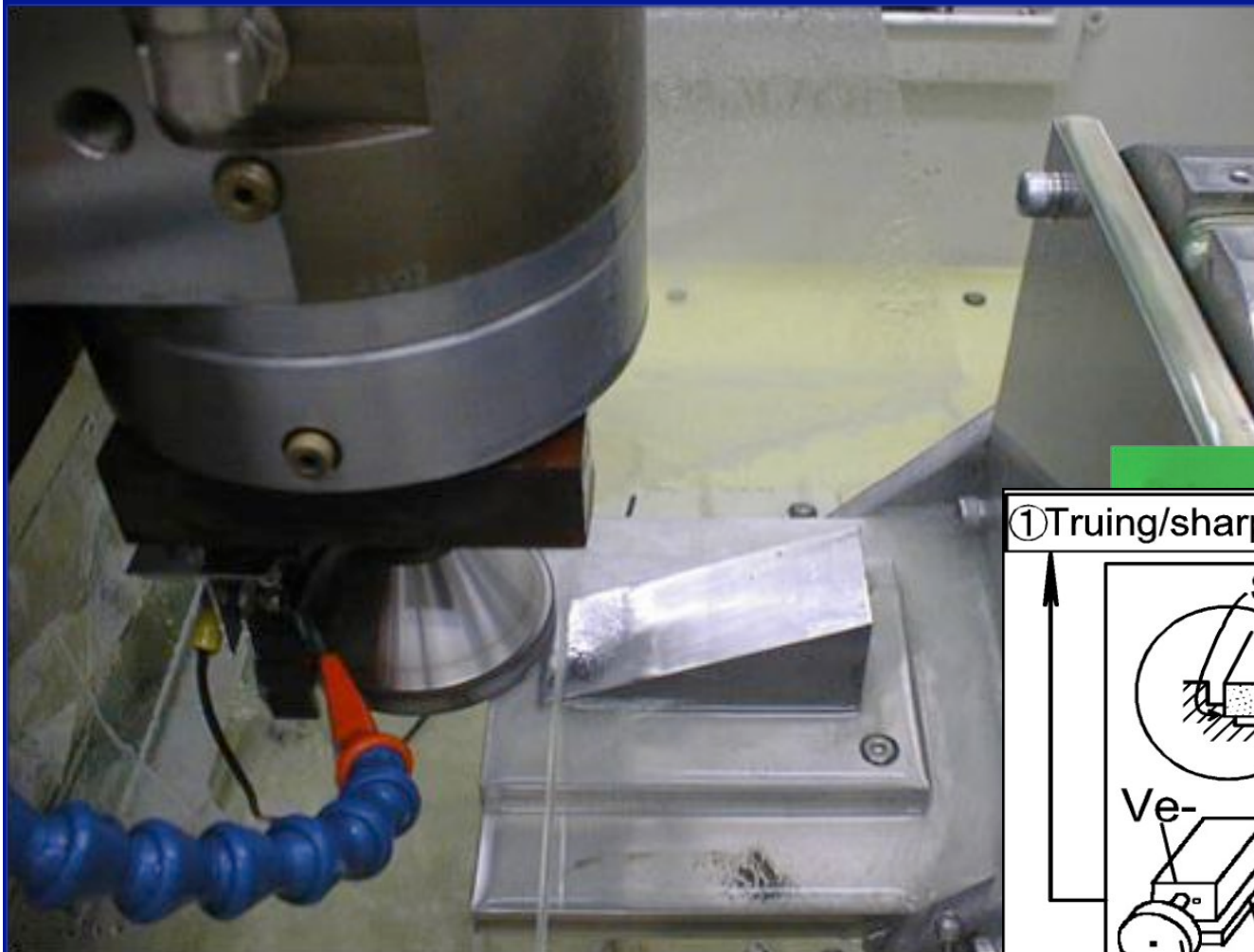
CISCO (J, H, K')

February 13, 2001

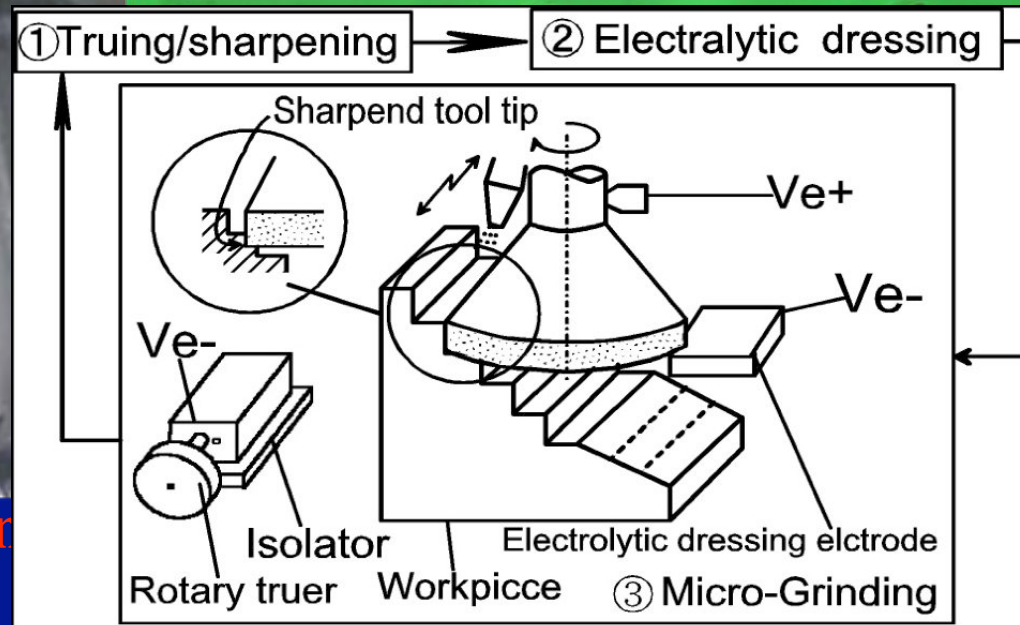
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Ge Immersion Grating for GIGMICS

(Germanium Immersion Grating Mid-Infrared Cryogenic Spectrograph)



Nano-precision machine and ELID grinding method.
30 × 30 × 72 [mm],
 $\alpha = 68.75^\circ$, $\Lambda = 600\mu\text{m}$

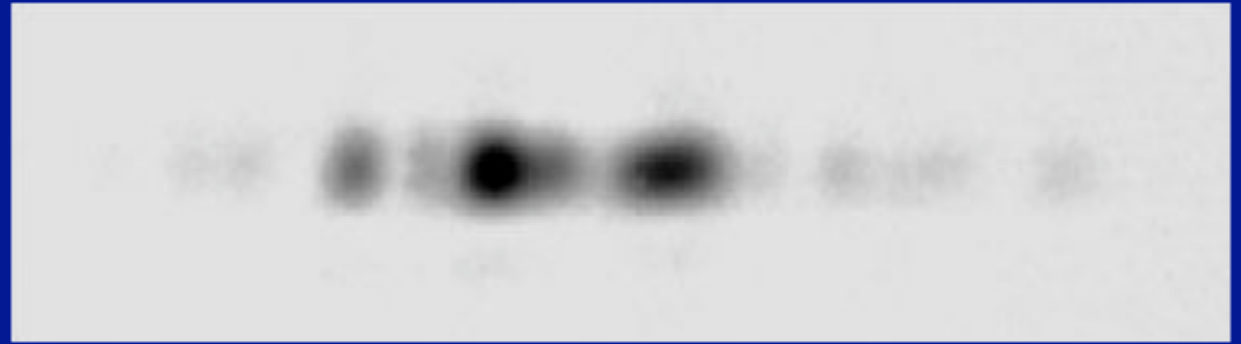
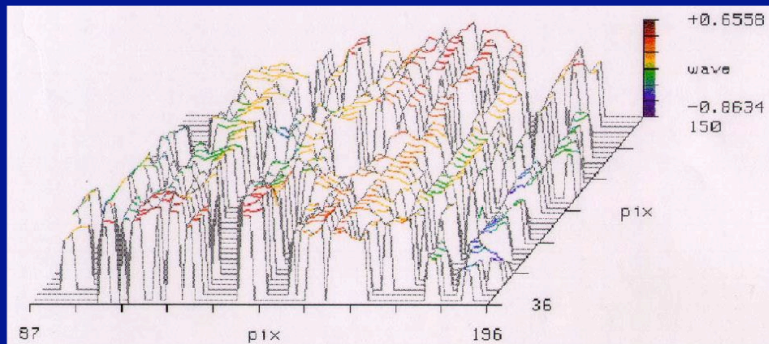


Spent about 400 hours for fabrication

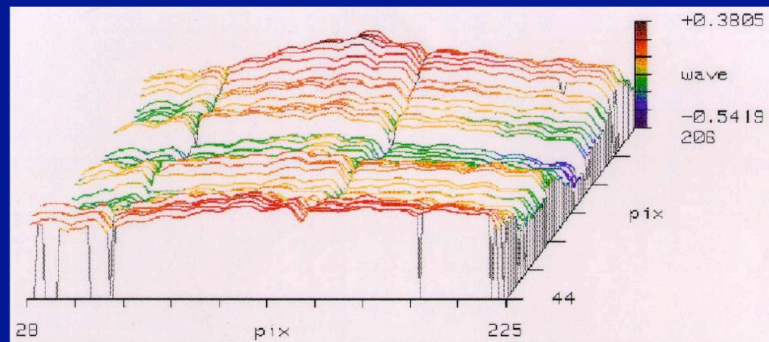
@RIKEN

(Ebizuka et. al. SPIE, 4842, 2003b)

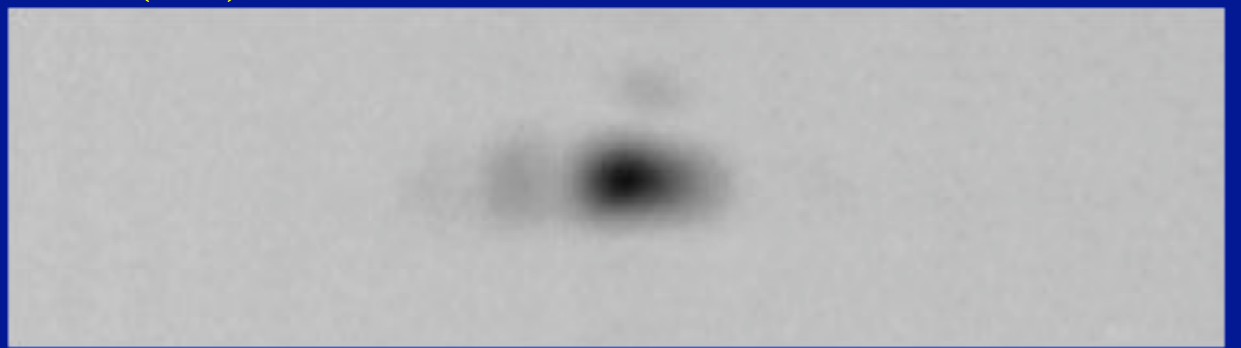
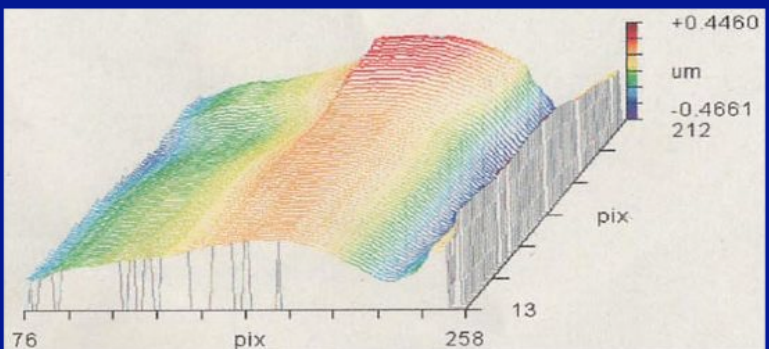
Wave front (633nm, left) and Far Field Images (10.6mm, right) of Immersion Gratings



The 3rd trial (GaAs), PV: 961nm, rms: 154nm

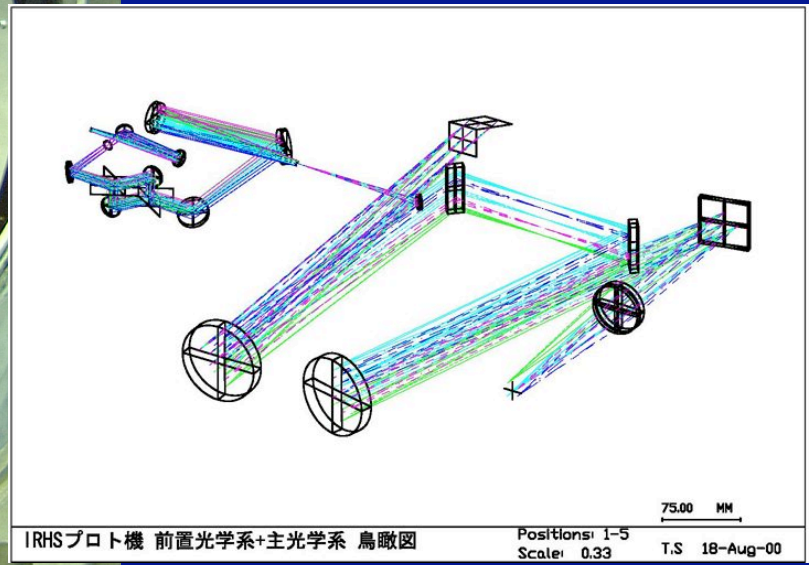
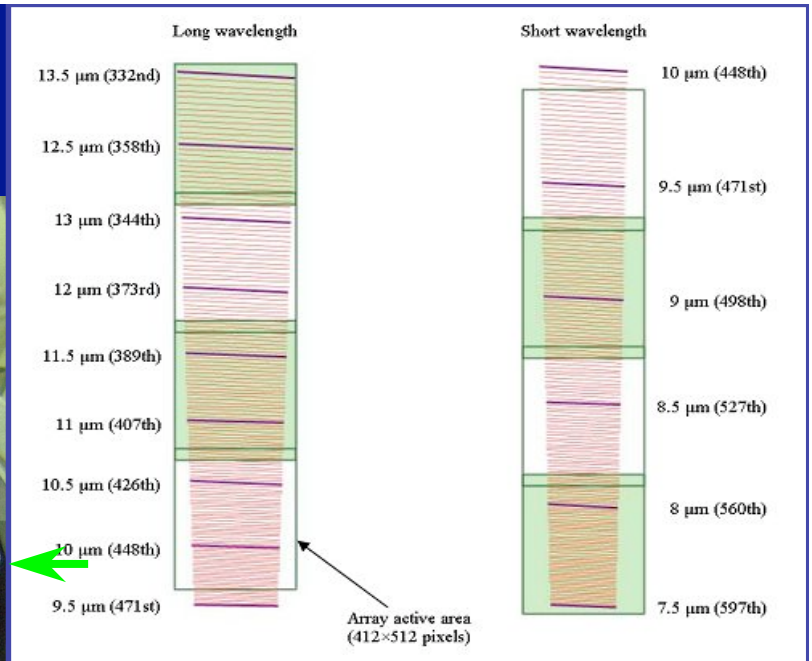
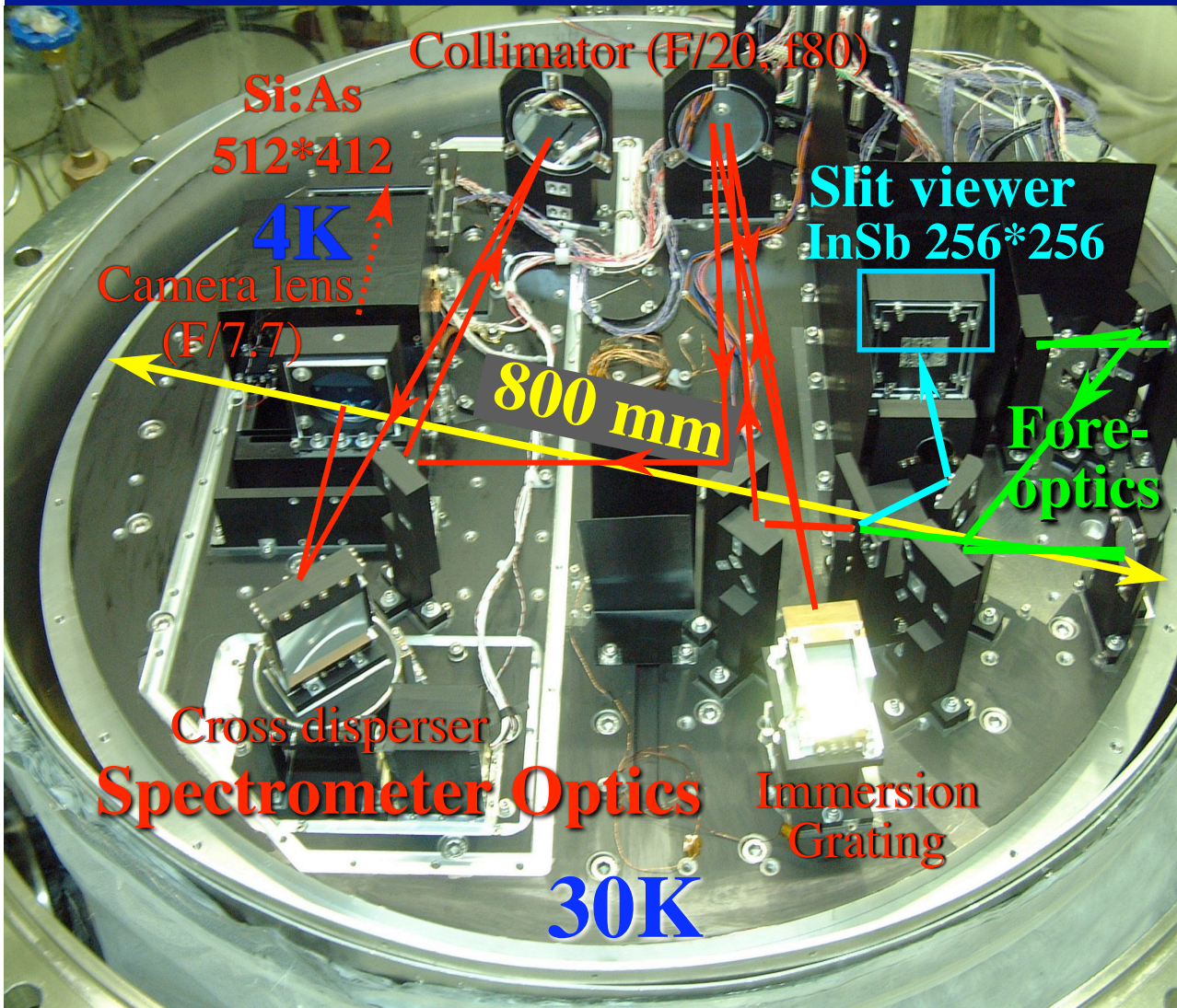


The 4th trial (Ge), PV: 583nm, rms: 87nm



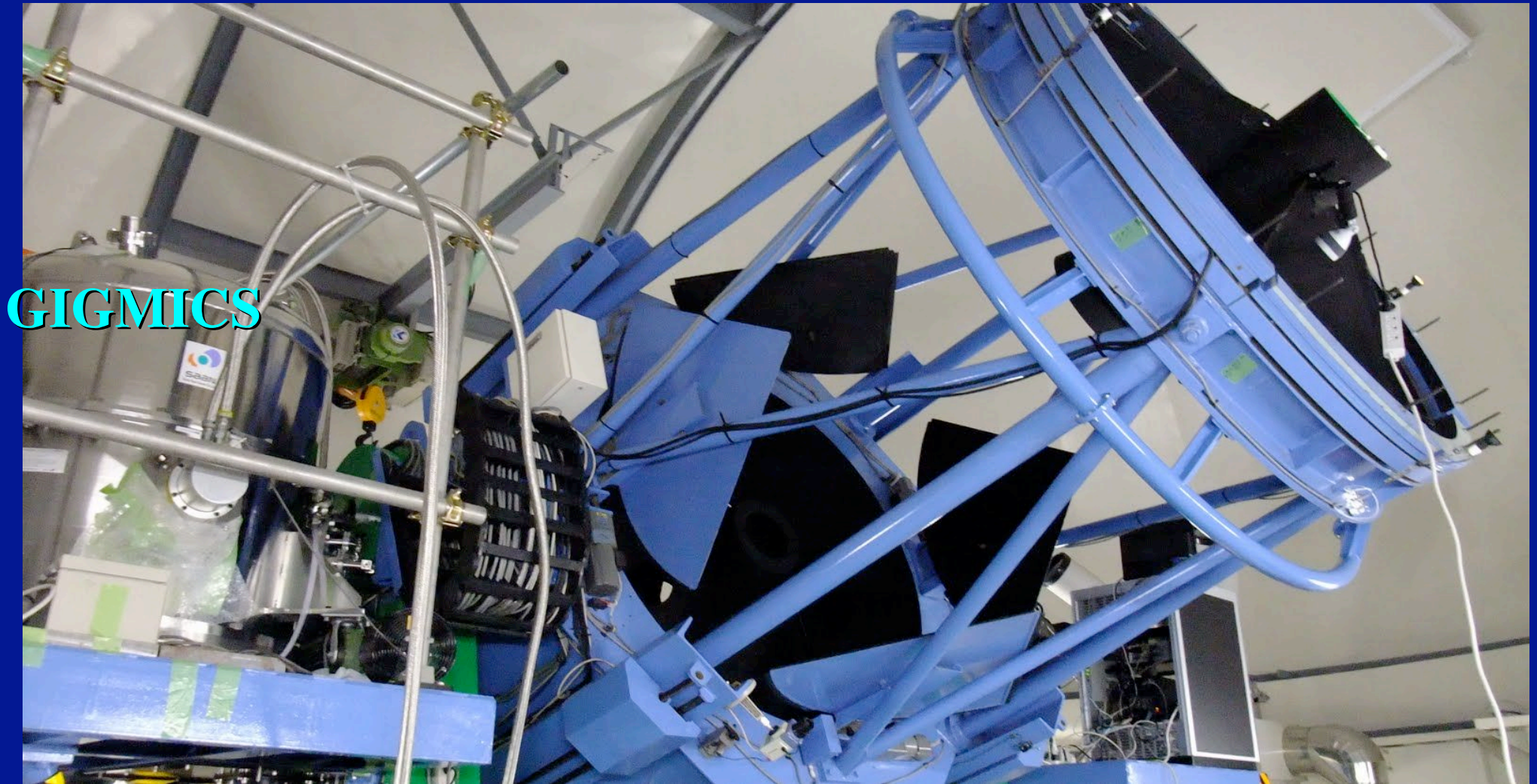
The 5th trial (Ge), PV: 577nm, rms: 107nm

GIGMICS



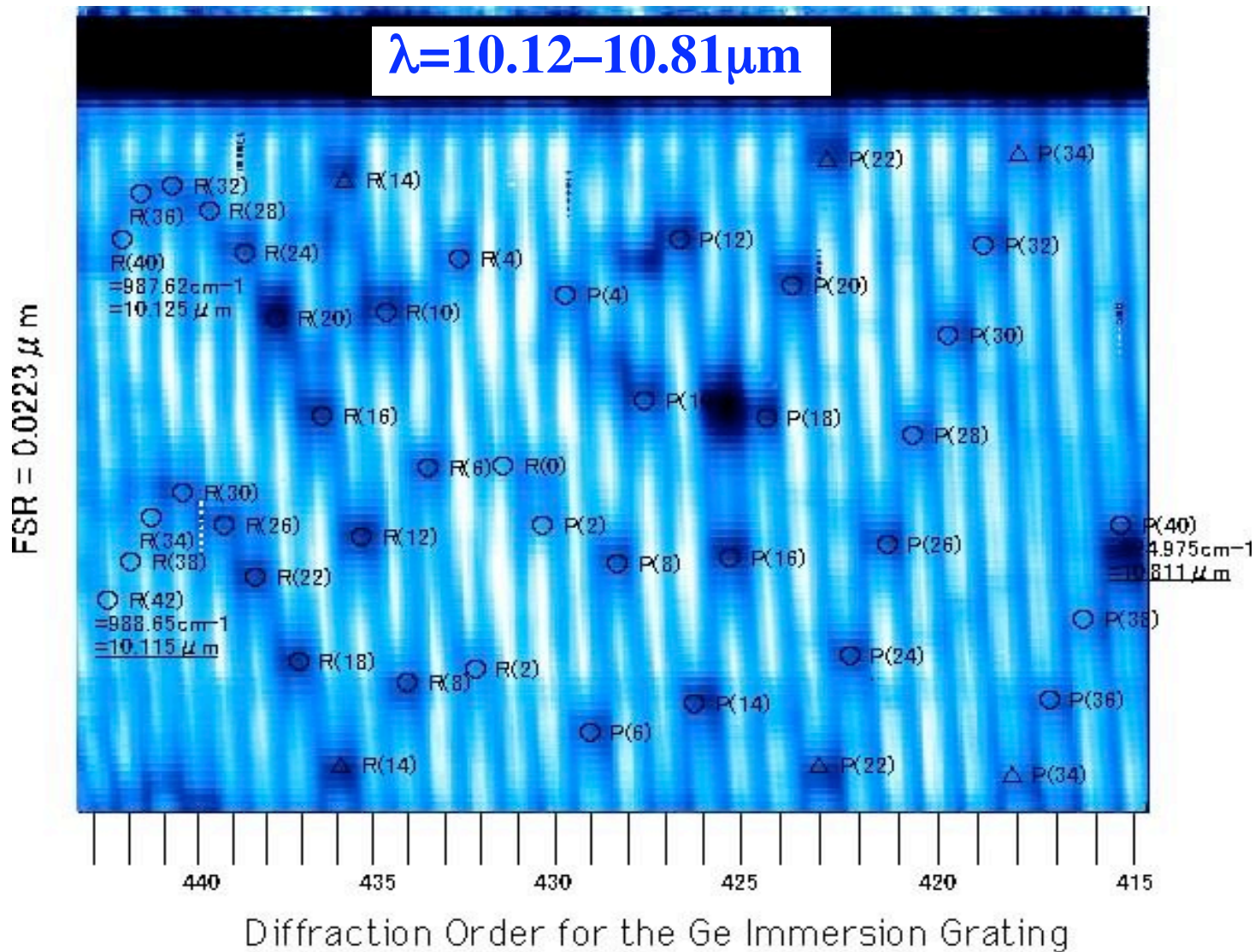
R~ 44,000@10 μm , developed by Hirahara lab., Nagoya Univ.
(Hirahara et. al., SPIE, 7735, 2010)

First Light Observation of GIGMICS



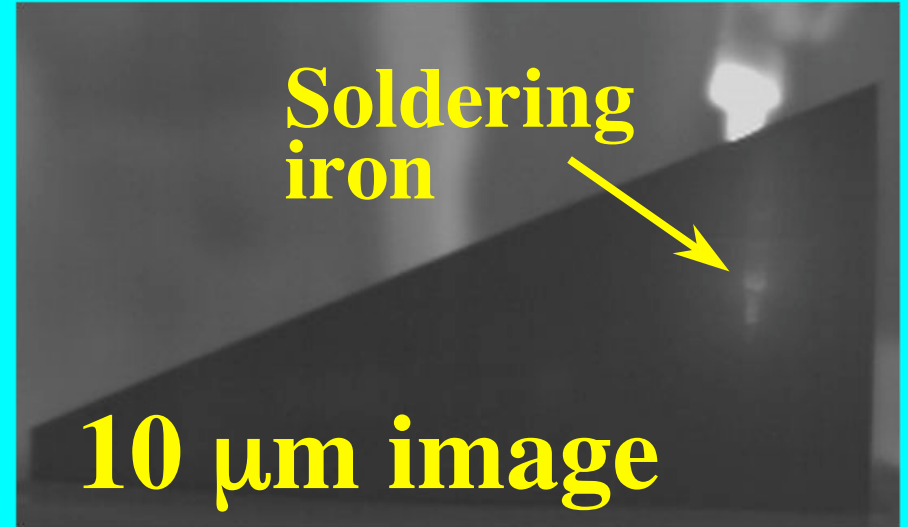
KANATA 1.5m telescope, Higashi-Hiroshima Observatory, Space Science Center Hiroshima Univ., Dec. 2010~Apr. 2011.

First Scientific Result (1): Venus

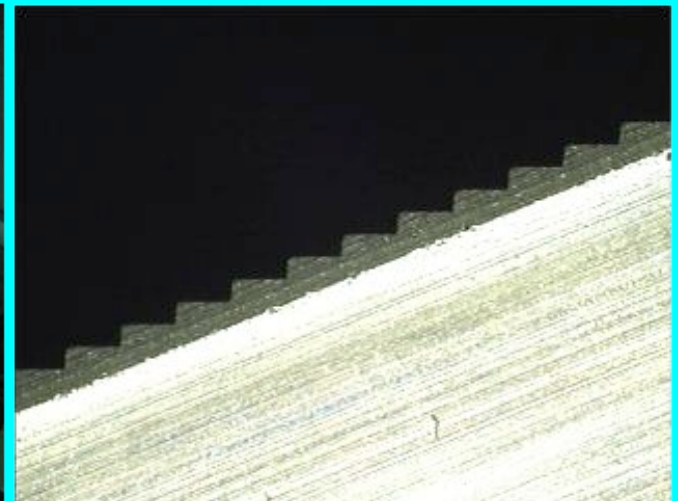
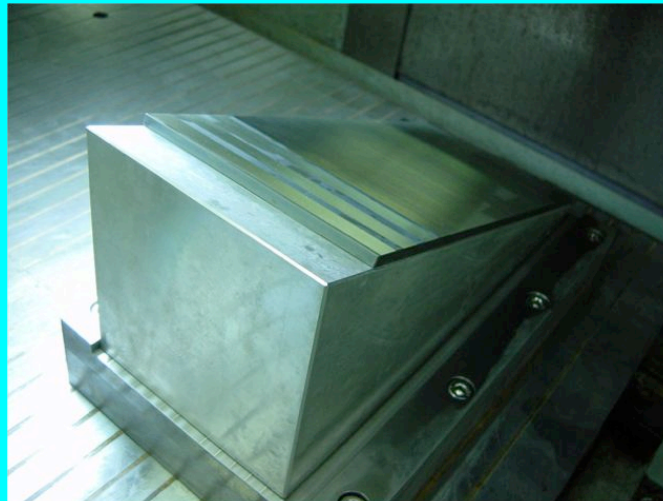


Absorption lines cannot be identified to the “telluric lines”.
→ CO₂ hot-band & isotopes from Venus.

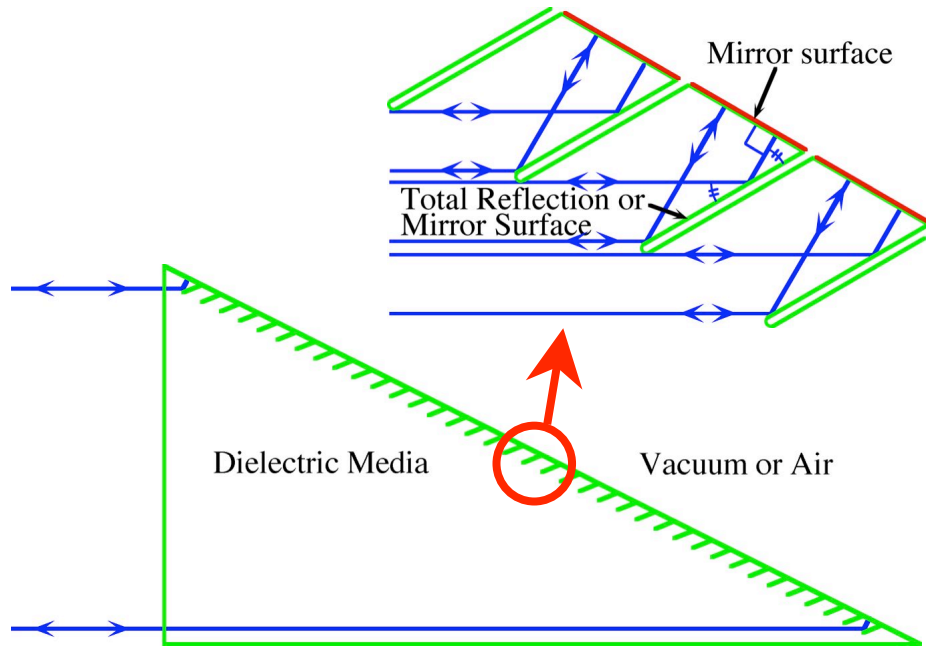
Trial Fabrications of Ge Immersion Grating for R~200,000



R~200,000@10μm → Size: 120 x 120 x 270 mm
→ Fabrication time: several 1,000 hours

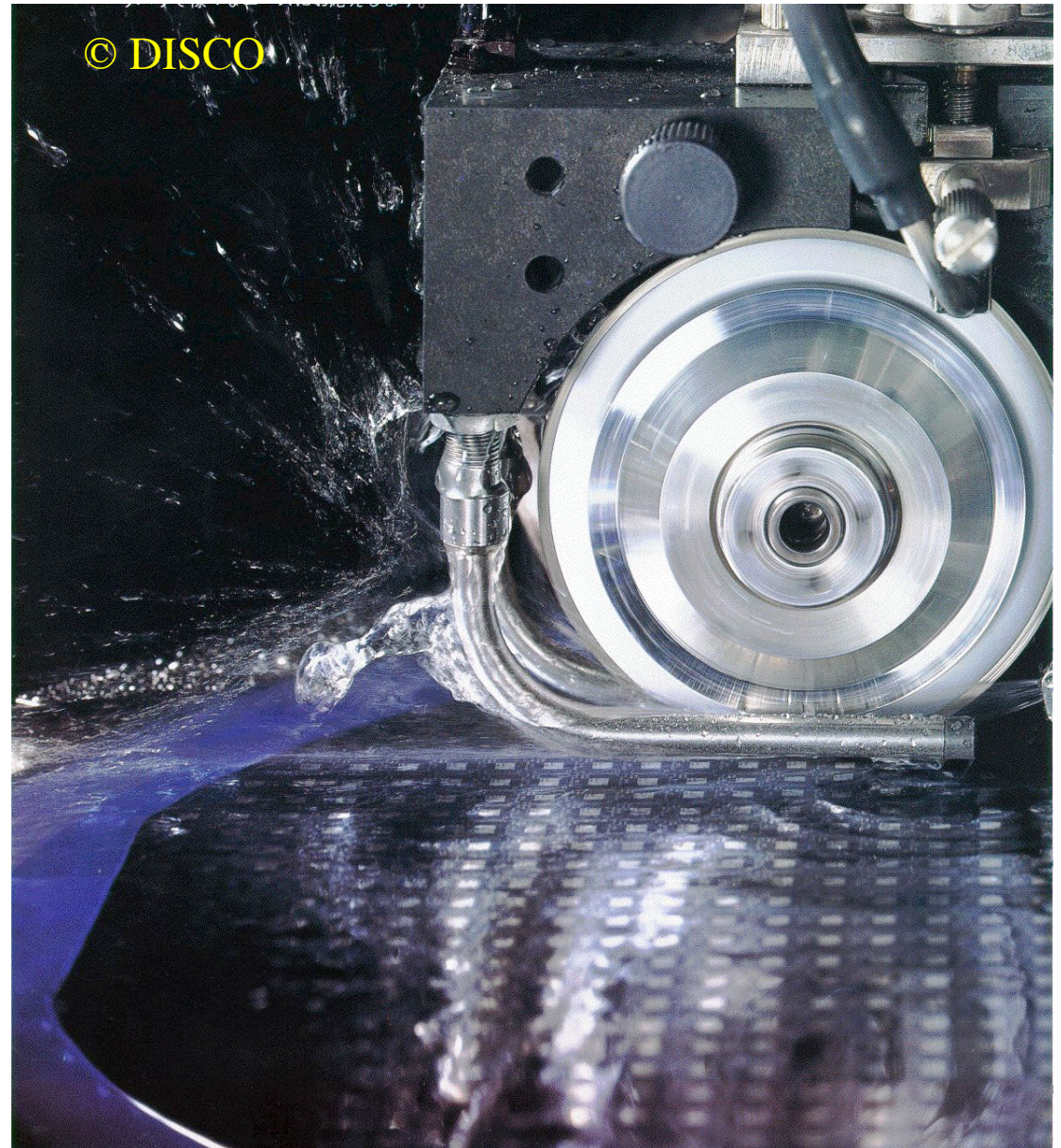


Quasi-Bragg Immersion Grating

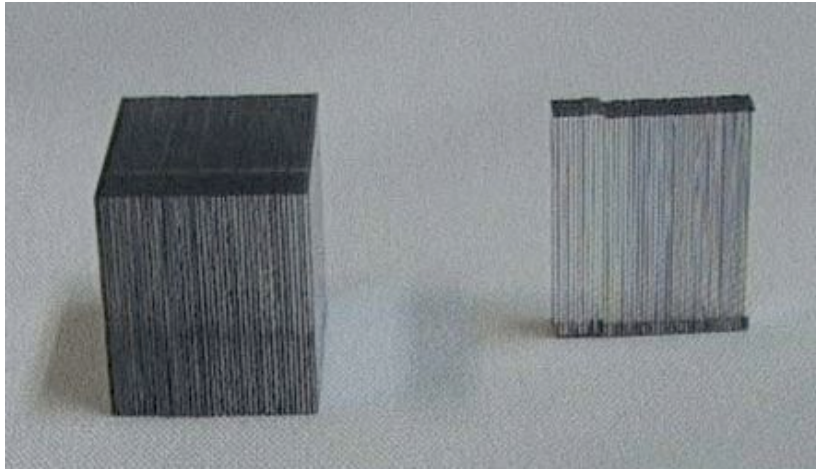


- **Machining of dicing saw makes smooth surface**
- **Easy tooling.**
- **Fabrication time for grating with 120 x 120 x 270 mm → Several 100 hours?**

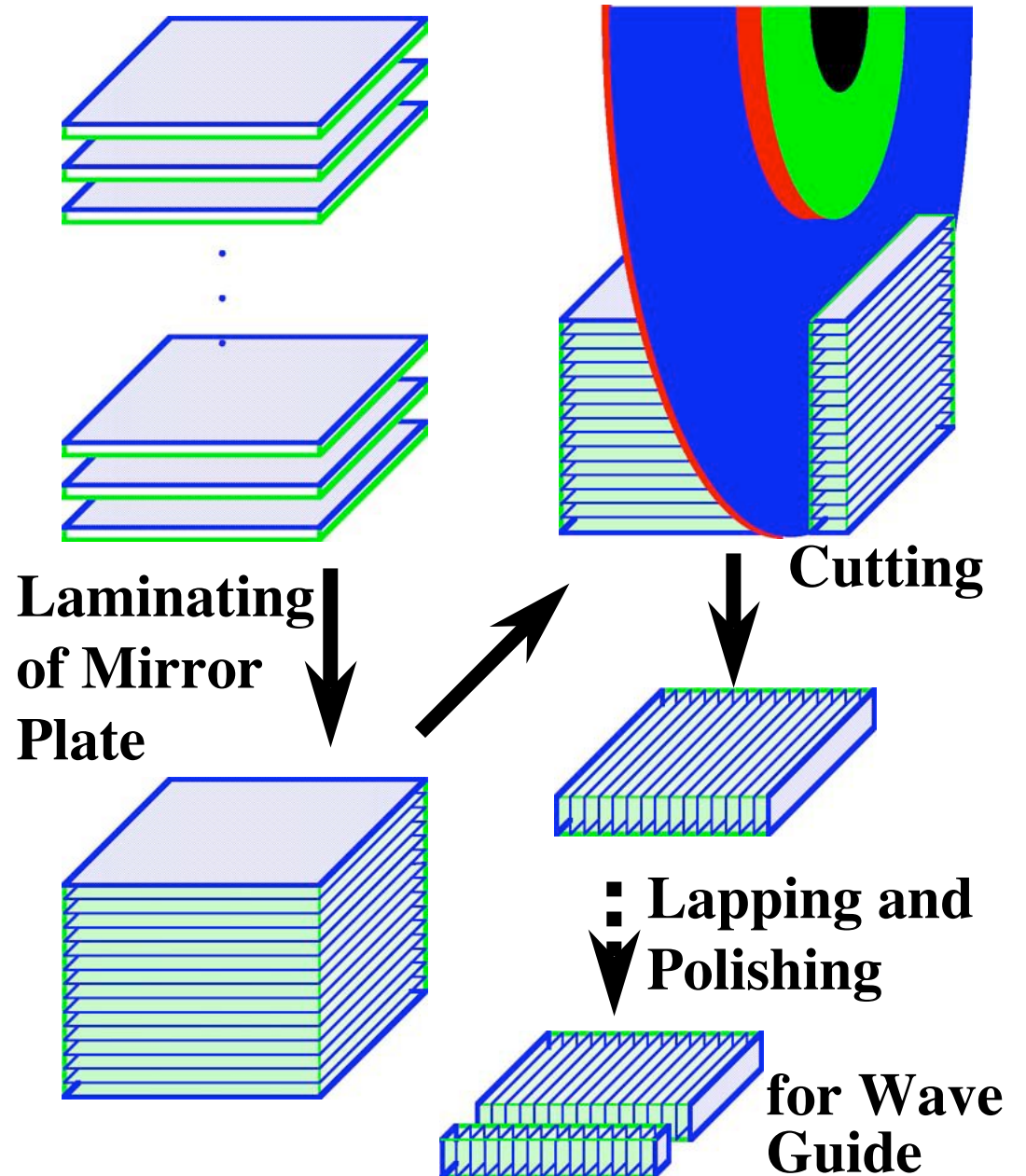
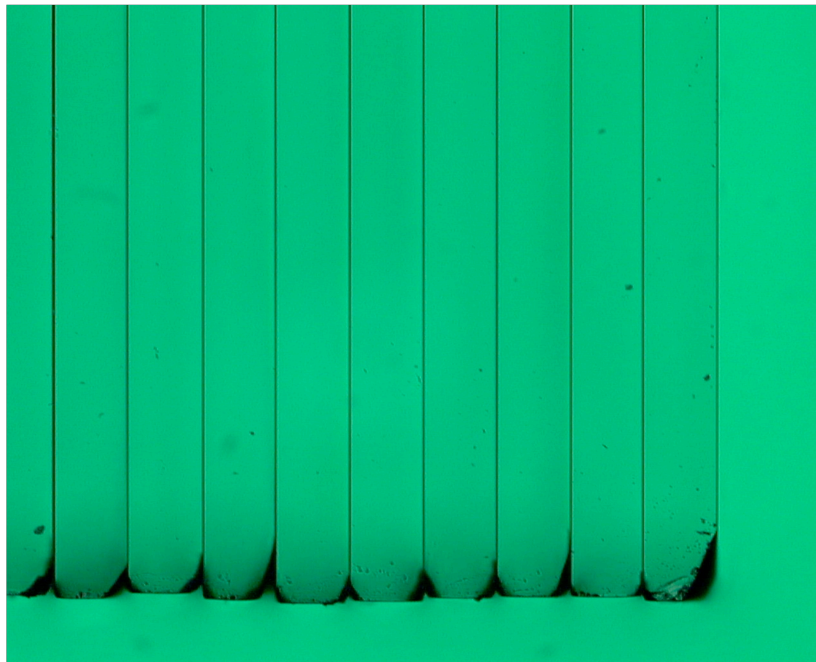
(Ebizuka et. al. SPIE, 6273, 2006)



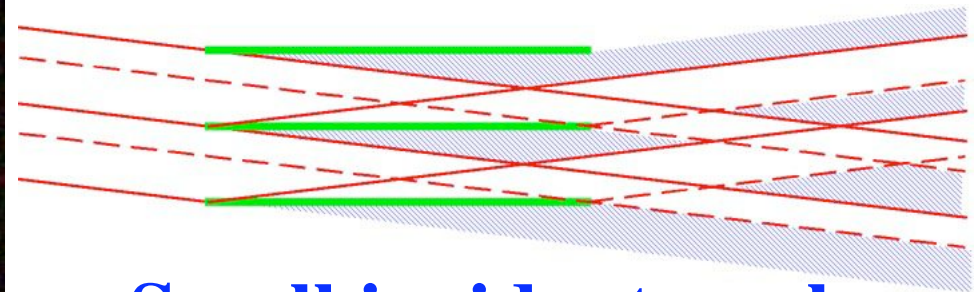
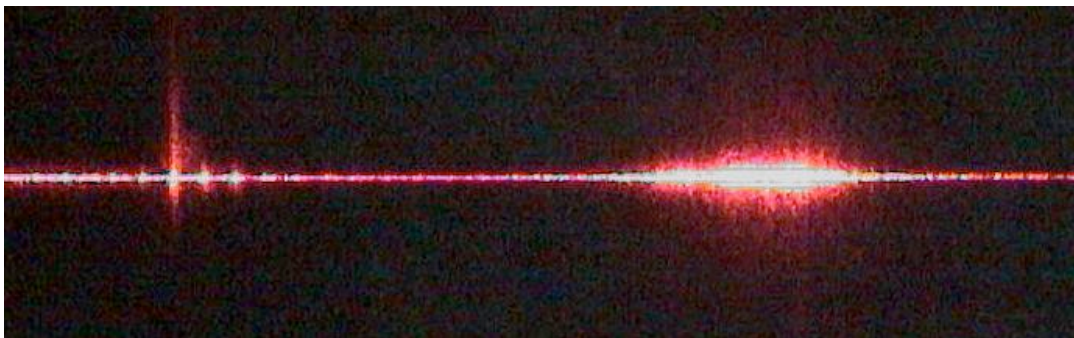
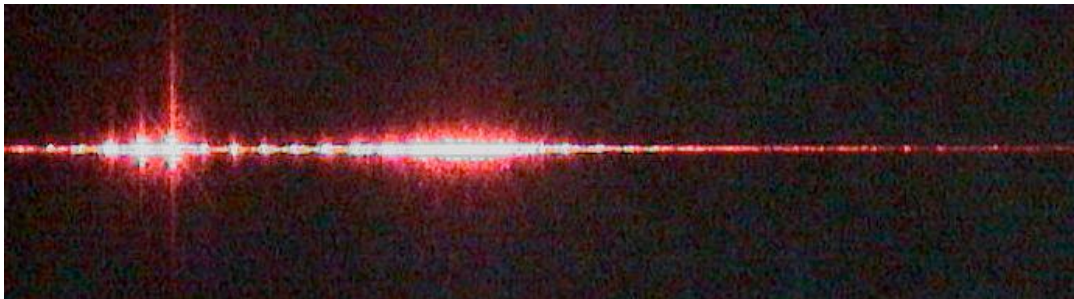
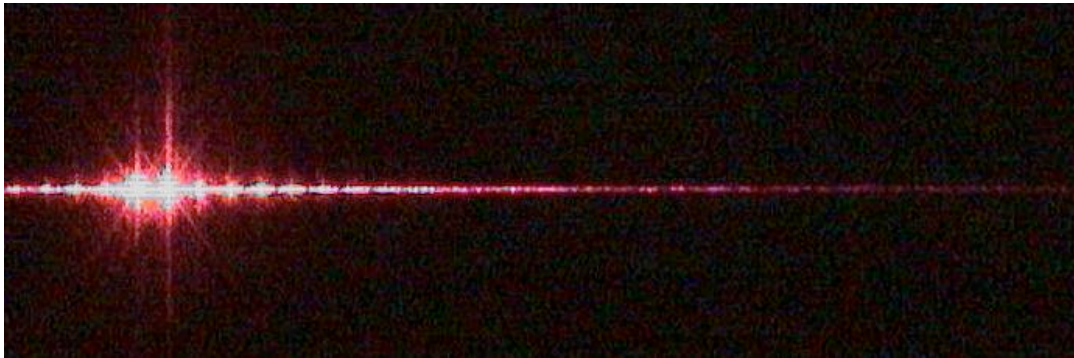
Trial Fabrication of Quasi-Bragg Grating



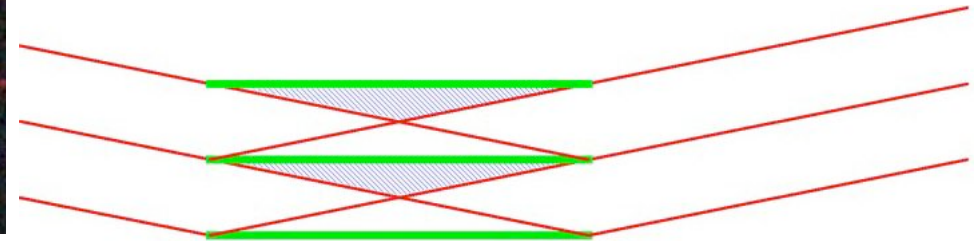
**A: 10 x 10 x 0.2 x 40 pcs (left),
B: 1.5 x 10 x 0.2 x 40 pcs (right)**



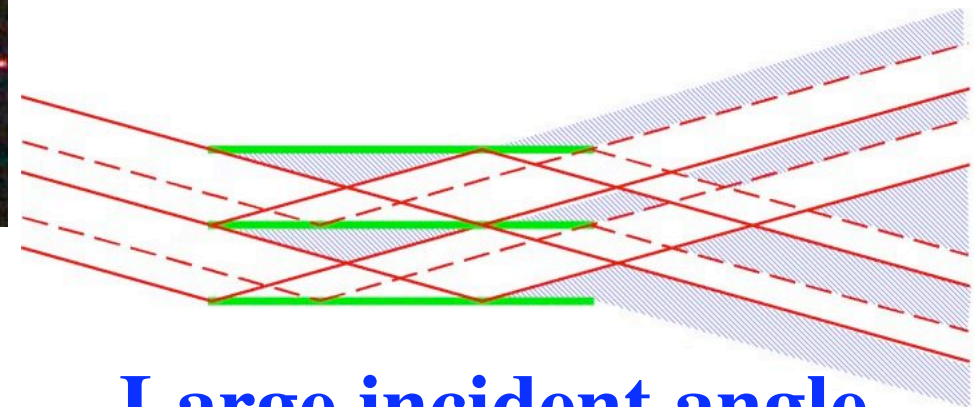
Diffraction of Quasi-Bragg Grating



Small incident angle



Ideal incident angle

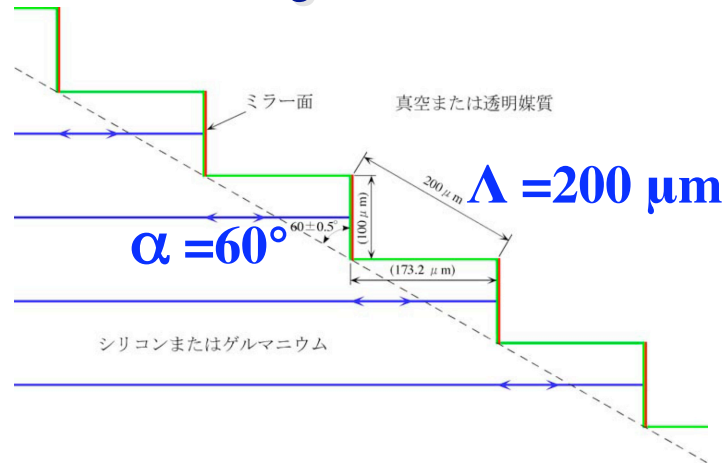


Large incident angle

Diffraction by quasi Bragg grating
(A type). $\theta = 0$ (top), $\theta = 0.6$ (middle),
 $\theta = 1.2$ (bottom).

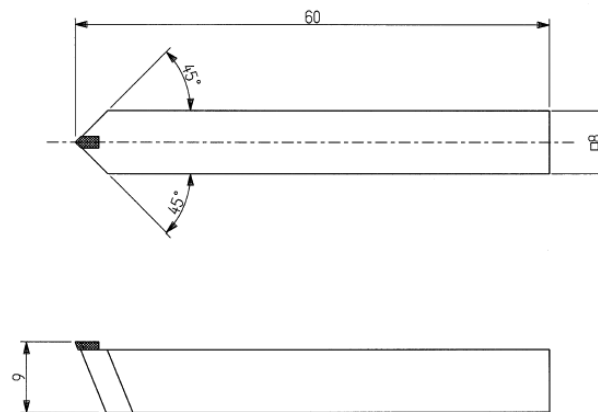
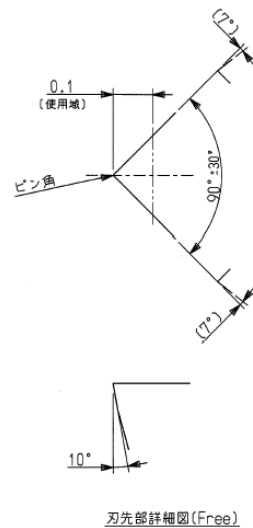
Spacing of mirror plates is imperfect.

Fabrication of Immersion Grating for Near IR by Means of Diamond Machining

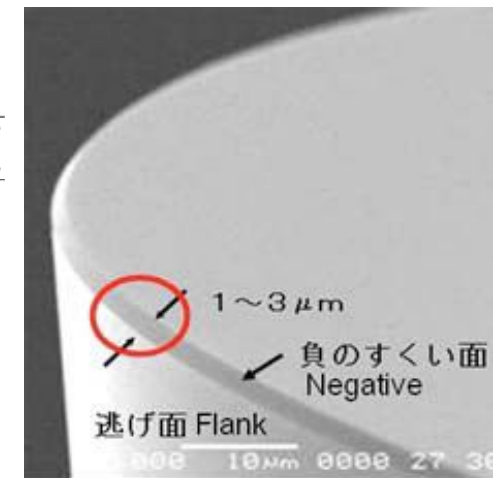


Specifications

Material	: Si, (Ge)
Wavelength range	: 1 ~ 2.5 μm
Groove period (Δ)	: 200 μm
Blaze angle (α)	: 60°



Note. 左右の切刃に硬脆材料用刃先処理を施す。



Diamond endmil

Diamond bite

Current and future works

- Trial fabrications of high aspect rectangular grating with duty ratio of 1 : 8~10.
- Trial fabrications of liquid crystal grating with high aspect ratio.
- Trial fabrications of immersion grating for near IR by means of novel diamond turning methods.
- Trial fabrications of quasi-Bragg immersion grating.

謝 辞

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**Thank you for your
kind attention!**