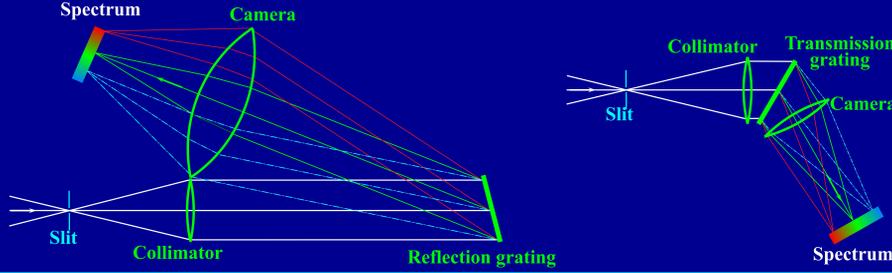


## Reflection and transmission grating

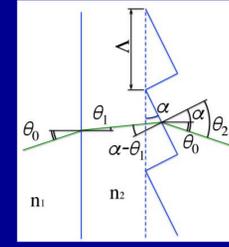
• Diameter of a camera lens exceeds maximum size ( $\phi 440$ ) of calcium fluoride if a reflection grating is used as the disperser.

→ Transmission grating can reduce size of the camera lens (→ total optical system).

→ Transmission grating is able to realize perfect Littrow mounting.



## Limitation of surface relief (SR) transmission grating



$\theta_2 < 90^\circ$   
 $n = 1.5, \theta_0 \leq 30^\circ$   
 $n = 1.8, \theta_0 \leq 36^\circ$   
 $n = 2.3, \theta_0 \leq 45^\circ$   
 $n = 3.0, \theta_0 \leq 54^\circ$   
**Diamond:**  
 $n = 2.46 @ 400\text{nm}$

SR transmission grating with saw tooth grooves is not feasible for the high-dispersion grating.

## VPH grating

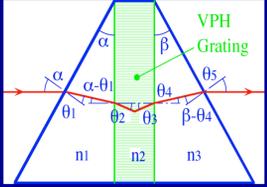
• VPH (Volume Phase Holographic) grating, in which refractive index is modulated sinusoidally achieves diffraction efficiency up to 100% for S or P polarization.

• VPH grating can not achieve high diffraction efficiency for natural and circular polarizations at high dispersion because characteristics of diffraction efficiencies are different between S and P polarizations.

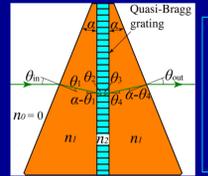
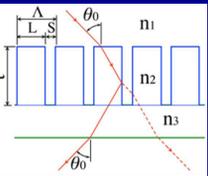
→ Birefringence VPH grating.

• Diffraction efficiencies of VPH grating decrease in higher orders.

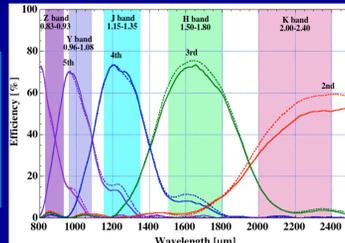
→ VPH grating is not feasible for an echelle grating.



## Volume binary (VB) grating for MOIRCS echelle grism



**MOIRCS echelle grism**  
 Slit width: 0.3"  
 5th, R = 4,630 @ 1.02  $\mu\text{m}$   
 4th, R = 4,420 @ 1.25  $\mu\text{m}$   
 3rd, R = 4,270 @ 1.65  $\mu\text{m}$

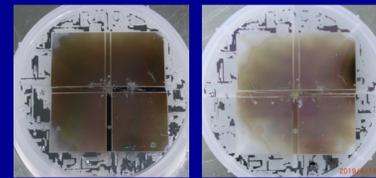
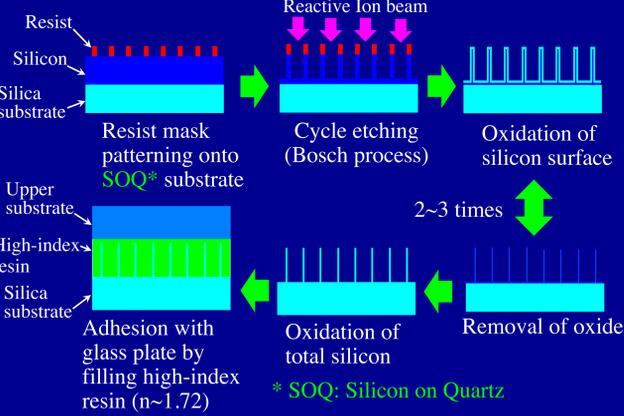


Diffraction efficiency of VB grating (RCWA). L&S = 4.6:0.5 [ $\mu\text{m}$ ],  $\theta_0 = 28.4^\circ$ ,  $n_1 = 1.33, n_2 = 1.6, n_3 = 1.6, t = 16 \mu\text{m}$ .

Schematic representation of volume binary grating.

Schematic representation of echelle grism.

## Fabrication process of VB grating



Before (left) and after (right) Si oxidation of VB grating fabricated in SOQ substrate.



Diffraction beam of VB grating

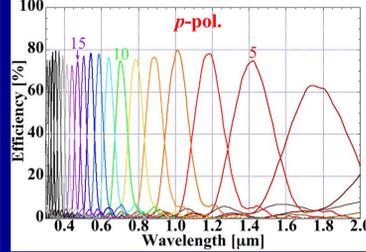
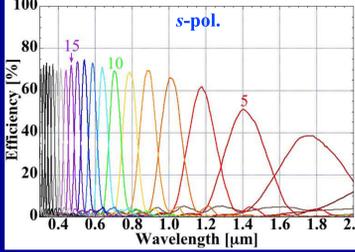
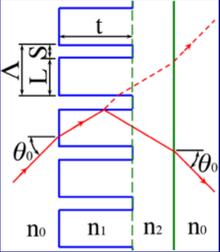
## Normalized specifications and performance of VB, SR and RFT gratings

AoI [°]	Order*	$n_1/n_0$	L:S	Duty	t [ $\lambda$ ]**	Aspect (S:t)	Peak eff. [%]	Bandwidth [ $\lambda$ ]***	Remarks
27.8	1	1.54	1:01	0.5	2	1:4	~90%	0.68	MOIRCS, K band
27.8	1	1.54	2:01	0.67	2.5	1:7.5	~93%	0.77	MOIRCS, K band
45	1	1.55	4:01	0.8	4	1:14	~95%	0.33	WFOS, etc.
28.4	3+	1.6/1.33	9:01	0.9	3	1:30	~75%	-	MOIRCS, echelle
45	7+	1.54	19:01	0.95	1.8	1:36	~75%	-	WFOS, VB grating
45	7+	-	-	-	-	-	~80%†	-	WFOS, SR reflection grating
45	7+	1.54	-	-	1.8	-	~83%	-	WFOS, RFT grating

\*Where + indicates additional orders. \*\*Normalized by grating period:  $\Lambda$ . \*\*\*Normalized by peak wavelength:  $\lambda_0$ . †Efficiency of p polarization is significantly shifted toward longer wavelength.

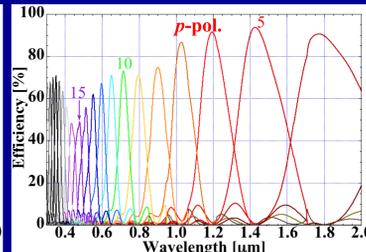
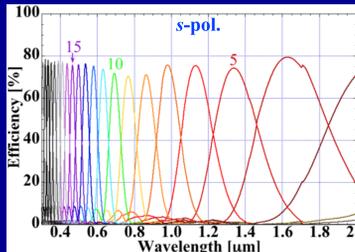
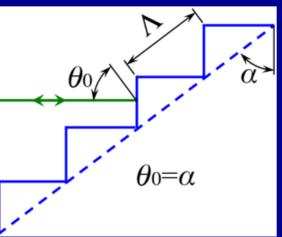
## VB, SR and RFT gratings for WFOS

### VB grating



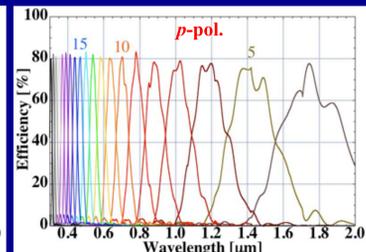
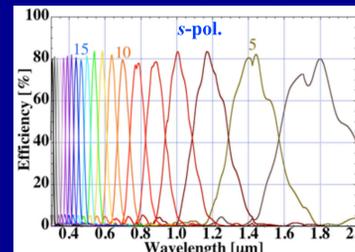
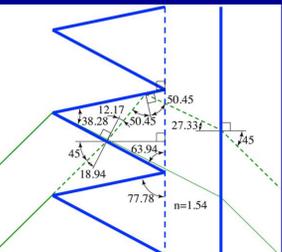
Schematic representation of VB grating (left), diffraction efficiencies of s (TE, middle) and p (TM, right) polarizations. VB grating of  $\theta_0 = 45^\circ$  without anti-reflection coating,  $n_1 = 1.0, n_2 = 1.54, \Lambda = 5 \mu\text{m}, L \& S = 4.75:0.25 [\mu\text{m}], t = 9 \mu\text{m}$ .

### Surface relief (SR) reflection grating



Schematic representation of SR grating with Littrow configuration. (left), diffraction efficiencies of s (TE, middle) and p (TM, right) polarizations\* for SR grating of  $\theta_0 = 45^\circ$  with Al mirror (thickness: 100 nm).

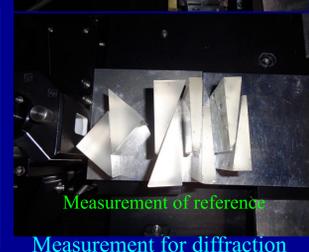
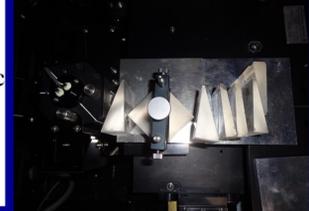
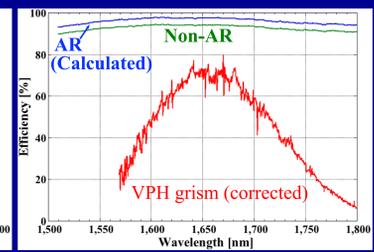
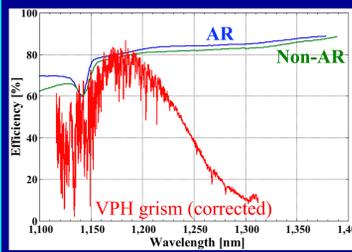
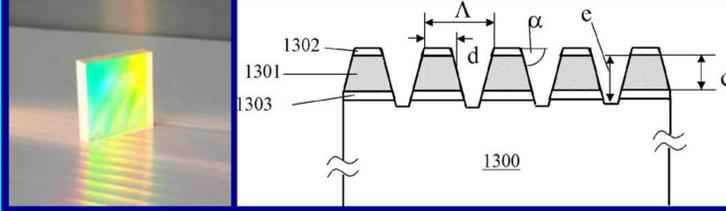
### Reflector facet transmission (RFT) grating



Beam propagation in RFT grating for  $\theta_0 = 45^\circ$  (left), diffraction efficiencies of s (TE, middle) and p (TM, right) polarizations of the RFT grating without anti-reflection coating.  $\Lambda = 5 \mu\text{m}, \theta_0 = 45^\circ, n = 1.54, \gamma = 38.3^\circ$ .

## LightSmyth Transmission Grating

for MOIRCS J and H band grisms instead of VPH grisms



Measurement for diffraction efficiency at blazed angle.

## Grism for MIMIZUKU



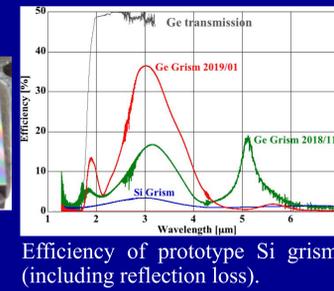
Fly cutting of Si grism



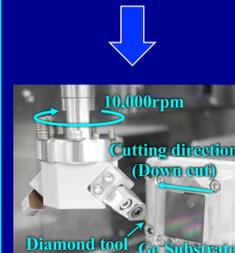
Microscope photograph of Si grism.



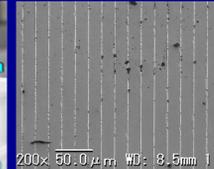
Si grism:  $\alpha = 4.2^\circ, \Lambda = 17.09 \mu\text{m}$ .



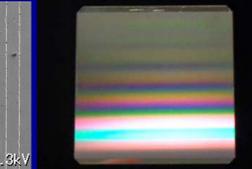
Efficiency of prototype Si grism (including reflection loss).



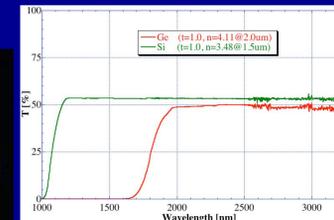
Fly cutting of Ge grism



SEM photograph of Ge grism.



Ge grism  $\alpha = 3.41^\circ, \Lambda = 17.07 \mu\text{m}$ .



Transmission of Si and Ge (including reflection loss).

## Summary

	Optimal Order	Eff. [%] ( $\lambda - \lambda_0 \mu\text{m}$ )	Status of development
VB grating	1 <sup>st</sup> ~	~ 95 (0.2~3.0)	Performed prototype of silica VB gratings by using SOQ substrate.
RFT grating	2 <sup>th</sup> ~	~ 80 (0.3~2.4)	Compared diffraction efficiency with VB and SR gratings, Planning the third trial fabrication in near future.
LightSmyth Grating	1 <sup>st</sup>	~ 100 (0.8~3.0)	Buy 3 transmission gratings of catalogue product for MOIRCS J band. Ordered transmission gratings for H band.
Si or Ge grism	1 <sup>st</sup>	~ 80 (1.2~14)	Performed direct diamond cutting of Si grisms. Planning fabrication of a Si and Ge grisms.

## Acknowledgements

We appreciate Mr. Kajiura of the Toyota Institute of Technology for their assistance on the trial fabrications of the VB gratings. We utilize facility of the Advanced Technology Center of the National Astronomical Observatory of Japan (NAOJ) for grating measurements, Nanotechnology Platform Japan of the Ministry of Education, Culture, Sports, Science and Technology of Japan (MEXT) and RIKEN Center for Emergent Matter Science, for grating fabrications and performance evaluations. This work is supported by the grant-in-aid of NAOJ for TMT strategic basic R & D.